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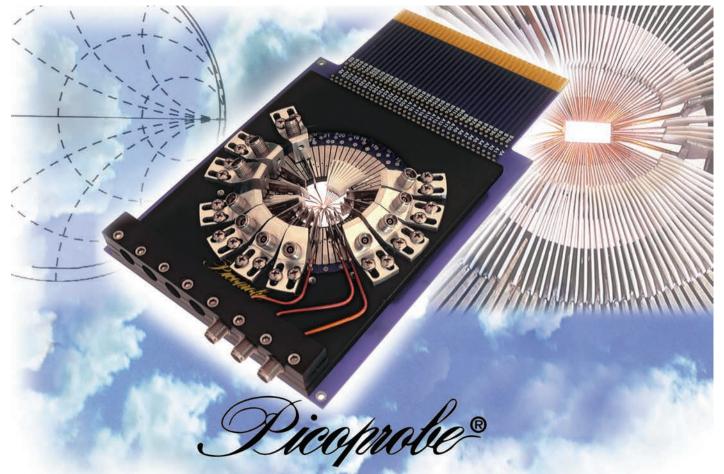
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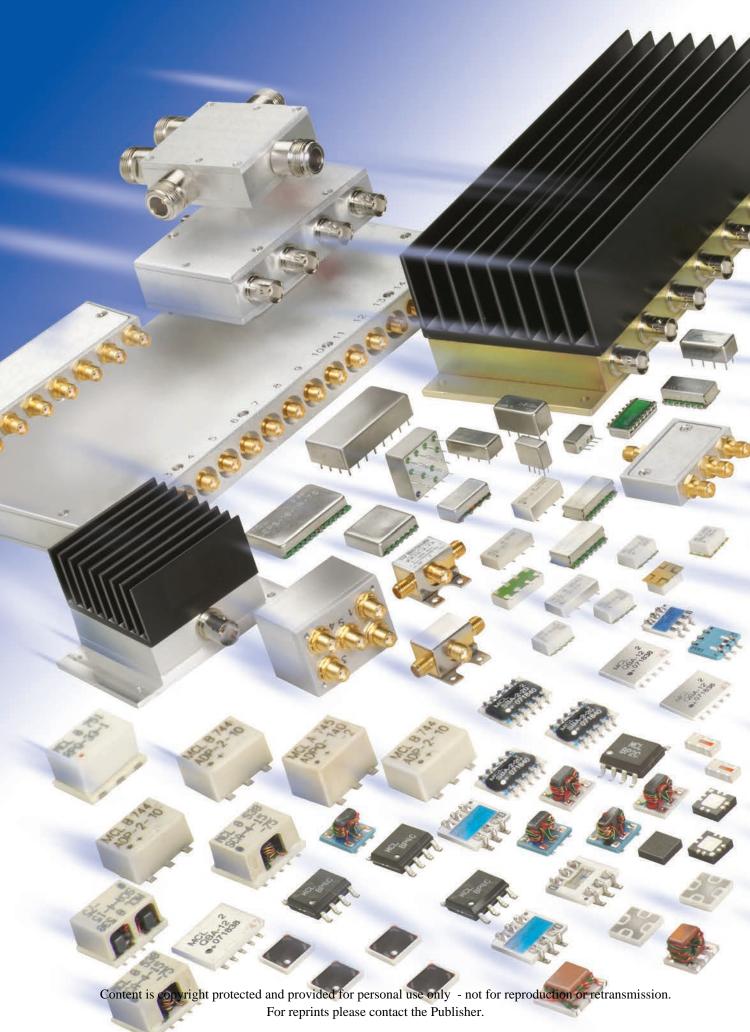


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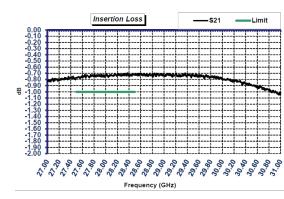
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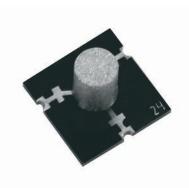


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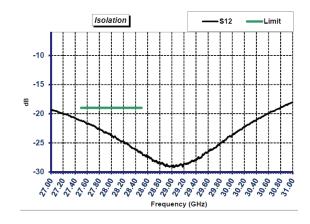




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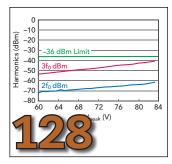












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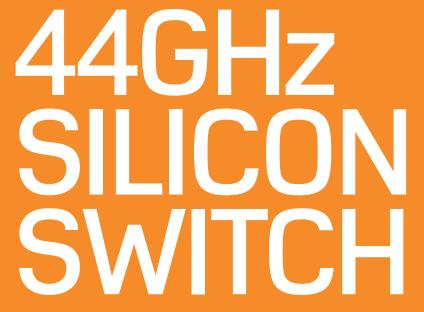


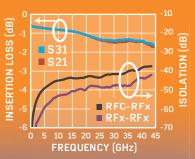
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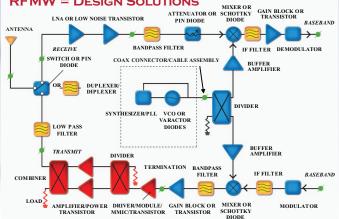
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Lars-Inge Sjöqvist, CEO of Gapwaves, talks about the company's unique waveguide technology and how it is being applied to mmWave antennas for such applications as 5G and automotive radar.



Web Survey

Which microwave industry is Spain's main strength?

Look for our multiple choice survey online at mwjournal.com/polls

June Survey What microwave innovation in 1958 had the most impact on the industry?

Microwave Journal begins publication (43%)

Bell Labs patent 2,866,949: Microwave circulators, isolators and branching filters (25%)

General Precision Laboratory patent 2,854,666: Planar microwave antenna array (14%)

General Precision Laboratory patent 2,830,276: Microwave rotary joint (11%)

Raytheon patent 2,833,657: Microwave irradiation of fruit juices (7%)

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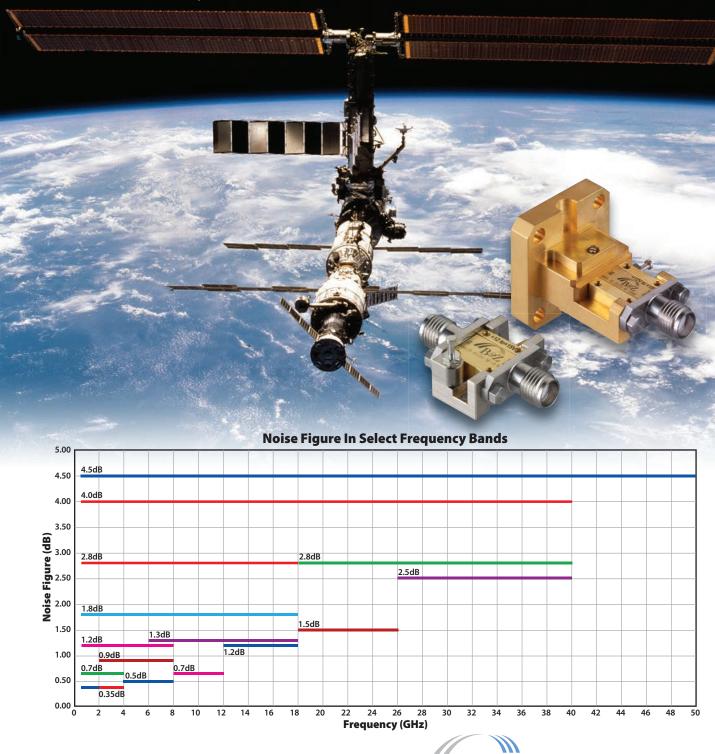
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August 27-Sept. 1, 2018 • Espoo, Finland www.congress2018.metamorphose-vi.org









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January 19-22, 2019 • Orlando, Fla. www.arftg.org

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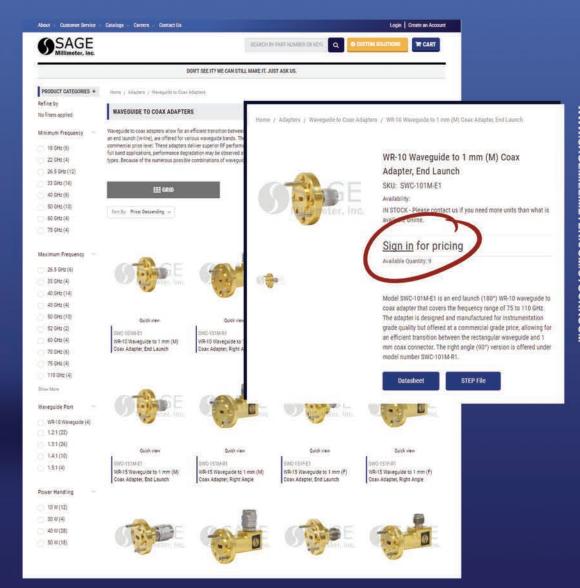
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European Cooperation in Defence Capabilities and Technology Research: Avoiding the Tower of Babel Effect

Ignacio Montiel Sánchez European Defence Agency, Brussels, Belgium

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he European Union (EU) is facing an unprecedented paradigm change regarding Defence Capabilities and Technology Research to be produced in collaboration between a variate set of Ministries of Defence (MoD), industries and universities. All these actors now work along with EU institutions which have the role to steer, fund, implement, monitor and support EU Member States in the Research and Capability fields. Because of this new context, numerous initiatives like the Permanent Structured Cooperation (PESCO) or the Coordinated Annual Review on Defence (CARD) are being launched. The most prominent one is the continuation of the EU Defence Fund for 2021-2027, with a proposed total amount of €13 billion from the EU budget apart from the national contributions, covering the Research and Capability windows.¹

These new initiatives are going to impact all the European Defence Capability and Technology Research ar-

eas including, by and large, the community addressed by the microwave industry. This article will highlight the challenges related to collaborative Research and Development (R&D), describe the existing frameworks and the lack of a common Overarching Technical Framework (OTF) under which an efficient and effective cooperation can occur.

To solve many of the issues connected to R&D cooperation for complex systems, the use of Interoperable Modular and Scalable Architectures (IMOSA) is proposed. IMOSA requires the establishment of Cooperation Frameworks covering Systems Engineering and Architectural views embracing Model Based Systems Engineering (MBSE) methodologies to decrease risks in design, development, validation and verification, avoiding in summary the Tower of Babel effect. The project Electro Optic and RF (EORF) sensors will be used to illustrate the IMOSA concept and related requirements.

EU INVESTMENT IN DEFENCE CAPABILITIES AND TECHNOLOGY RESEARCH COOPERATION

One of the most prevalent challenges that cooperative projects face at international level is maintaining reliable and accurate communication between different parties. That communication issue can affect very complex systems projects formed by disparate teams from different countries and cultures, implying a high risk of failure.

A good metaphor to refer to this challenge is the Tower of Babel myth. In Genesis 11:1-9 of the Bible, it is explained how God scattered people from Babylonia over all the earth by confusing their language. In order to diminish the Tower of Babel effect, it is important to adopt and use common frameworks. MBSE can significantly de-risk cooperation projects. To establish it, a common Systems Engineering and Architectural Framework (SE/AF) is required, including technology and

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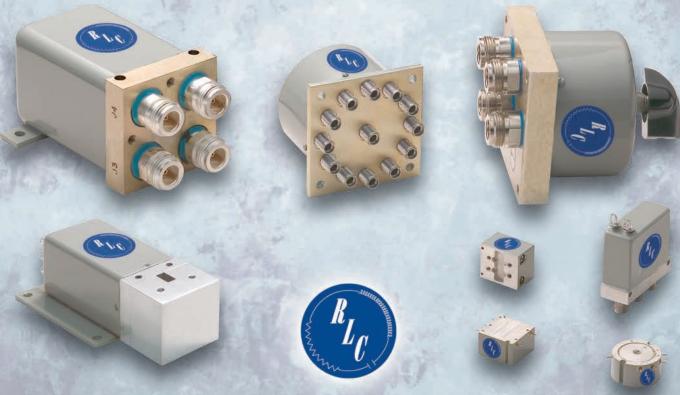
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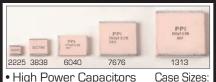
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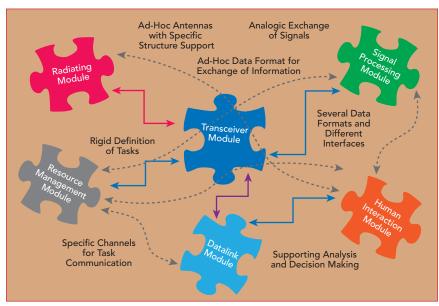


Fig. 1 Traditional systems exemplification.

capability taxonomies together with agreed ontologies.

Some of the challenges faced by international cooperation are:

a) Exploitation: The bridge from research results to exploitation required to increase the impact of the investment made in Research Programmes is one of the main issues to solve. The need to link the end-users to the projects for further uptake is not new. Even if operational users can be consulted and involved in the process, several points remain open as procurement is rarely linked to research projects. This is the well-known "Valley of Death" 2 issue occurring to the research results which cannot follow the path to exploitation.

b) Intellectual Property Rights (IPR): IPR sharing rules of Research Programmes sometimes preclude achieving cooperative results close to the exploitation path.³ Involved companies or entities are sceptical to share their core IPR requested to develop complex systems within consortia. This is needed to allow working together and to facilitate the integration of the different components of the System. Consequently, meaningful cooperation is preferred not to be faced under these kind of schemes.

c) Complexity: With regard to the System's needs, the ever-increasing complexity of battlefield scenarios results in requirements

for disparate interoperable systems from different manufactures to be integrated into coalition operations where modifications and updates have to be quickly implemented, with verification and acceptance tests being planned as part of a fast V-cycle. In such a complex development environment, information degradation is likely to happen as it circulates between very different partner companies used in different procedures, cultures, languages, expertise, insufficient requirements and results understanding, rounding errors, etc.

- d) Status Quo: Some characteristics of the currently used system architectures are (see Figure 1):
- Duration from months to years of the certification of new integrated capabilities.
- High vulnerability to cyber threats because of too slow implementation of updates.
- Long time to update and test causing systems rigidity.
- High cost of upgrade due to increasing licensing fees provoking sustainment challenges.
- Software duplication with more than 80 percent communality estimation.
- Hardware duplication like redundancy of servers and clients.

THE IMOSA CONCEPT

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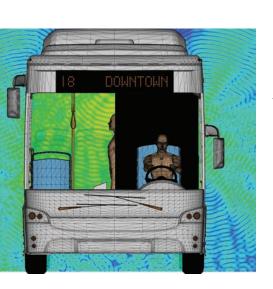


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| GC2075A | 2 | 2.1 | -15 | -35 | 45 | -50 |
| GC3075A | 3 | 2.1 | -10 | -30 | -30 | 45 |
| GC4075A | 4 | 2.1 | -10 | -35 | -35 | 40 |
| GC5075A | 5 | 2.1 | -5 | -20 | -25 | -35 |

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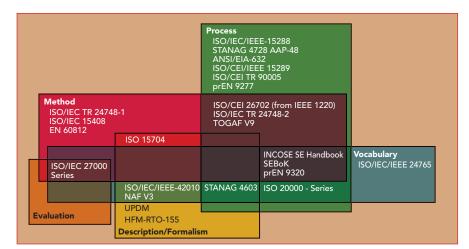


Fig. 2 EG20 Characterisation MAP for identified standards–Summary Table.

tioned above being based on the following aspects:

- a) Modularity defines the way to design a system based on elements named Building Blocks (BB) which are described by their functionality and interfaces with other BB, the system as a whole and with other systems as well. The great advantage in research programmes is the possibility to isolate the work on BBs that can be easily integrated later if compliant with the specifications.
- b) Scalability implies that different amounts of the same hardware or software items-BBs—are used to create systems with increased performance or additional capabilities. Both architecture and BBs should have the scalability character from their definition and design. The character of scalability would suit very well to a research programme as the system can be validated at a reduced size and later escalated for an operational system. The degree of granularity of BB is a fundamental issue in the design.
- c) Interoperability is ensured through the definition of these architectures under a defined SE/AF considering the Life Cycle of the Systems and a defined verification and validation scheme. The description of the different architectural views needed by the several actors and stakeholders in the process can support in a much better way the understanding and collaboration of all communities.

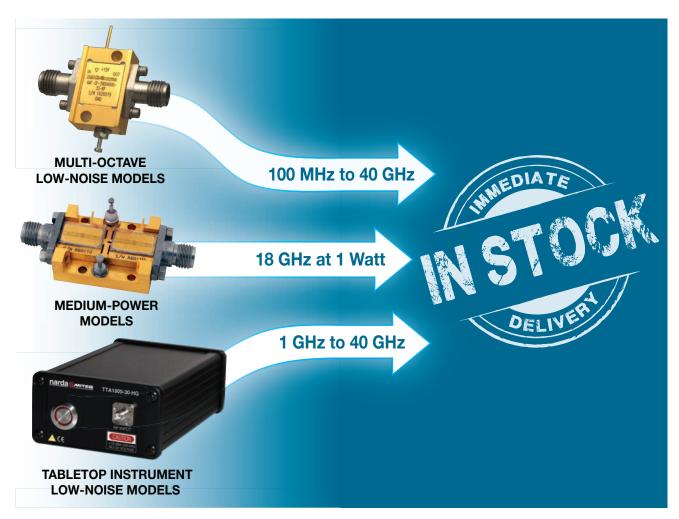
The advantages of using IMOSA

- in a Cooperative Research Programme can be summarized in the following:
- It allows for collaboration projects facilitating the development of complex systems while protecting the IPR of the partners.
- It could be a solution to ensure participation of smaller parties without a strong Defence Technological and Industrial base.
- It would create a level playing field for all suppliers and partners independent of their size and influence.
- The prime contractors from different countries could benefit from the investment in developing IMOSA and then have the possibility to national implementations integrating specific BBs when demanded by a certain procurement programme.
- It allows for more cost-effective procurement based on a truly competitive landscape in possible follow-on projects.
- Through-life maintenance and upgrades can be open to competition as the future integration can be realized without any constraints.
- Systems can be redesigned and upgraded in a dynamic way, keeping up with the commercial world and the innovation enabled by new technologies.

The challenges to introduce IMOSA are mainly:

- The architecture has to be robust and sound as there is a trade-off amongst characteristics given that flexibility, modularity and scalability could come at the cost of reduced performance.
- Lack of conviction from primes

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of the need to open participation to all partners including SMEs and international collaboration. Most of the benefits seem to be for governments rather than industry but, the need to work in cooperation and the possibility to integrate innovative and cost-effective solutions for BBs has to be considered by primes.

- Ownership, definition and evaluation of the desired architectures should come from collaboration between industries and governments in an integrated approach.
- Once the degree of openness and availability of the architectures is agreed, the rules and agreements embracing the use of IMOSA for subsequent contracts must be established.











HOW TO IMPLEMENT THE IMOSA CONCEPT? WHAT SE/AF SHOULD BE CONSIDERED FOR THE OTF?

To undertake the IMOSA concept, it is required to select and adopt specific SE/AF. SE is an interdisciplinary approach governing the total technical and managerial effort required to transform a set of customer needs, expectations and constraints into a solution and to support that solution throughout its life.4 To establish the way of working in SE several frameworks exist like NASA and EIA632 (freely available), ISO15288 and IEEE 1220 (both requiring subscriptions) and INCOSE (an extension of ISO 15288) which requires membership.

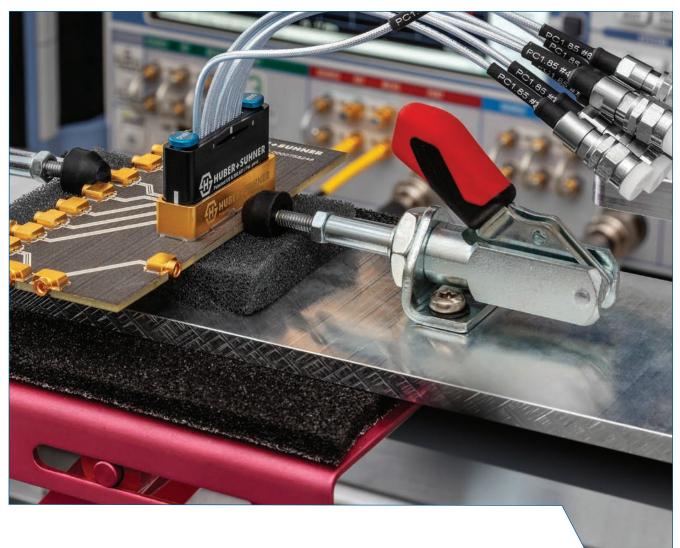
SE grows more necessary as the system becomes more complex. Take the example of development and integration of a swarm of heterogeneous UAVs equipped with different sets of payloads and providing ISR functions. Its design, development and operation involve such complexity that is not possible to manage without SE/AF. The first step is to create their architecture (or Enterprise Architecture) as a structured abstraction of reality and its detailed representation with the correct level of granularity in a way that is commonly agreed and unambiguous.

AF provides the guidance and rules for developing, representing and understanding comparable architectures based on common denominators and multinational boundaries. Several AF exist like Zachman, DoDAF, MODAF, TOGAF, IAF, FEAF, TEAF, SCOR, NAF, UAF.⁵ Those structured engineering approaches are requested, not only to clarify how things are designed, built and maintained, but as well to get a common description understandable by all the stakeholders and to ensure interoperability through a set of standards and specific methodologies.

The complexity and variety of standards can be displayed in the representation of *Figure 2* from the European Defence Standards Reference System (EDSTAR) which is a repository of references to "best practice" standards and "standard-like" specifications.⁶

Current advances in Defence show a strong interest on making an over-





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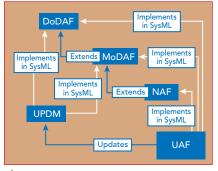
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arching, compatible and interoperable Unified Architecture Framework (UAF) as a way to link with other AFs. The relationship to be made between DoDAF, MoDAF, NAF and UAF⁷ can be seen in *Figure 3*.

The wish from part of the Defence community would be to align the evolutions of MODAF v1.2.004 (U.K.) and MODEM v1.1 (MODAF Metamodel) into NAFv4.0 (NATO). That would be the basis of UAF v1.0 as an overarching framework which would be complemented from DoDAF 2.x (U.S. DoD) and DNDAF (Canada). This would be supported with the modelling language for Enterprise Architecture Archimate.

ISO/IEC/IEEE42010⁸ provides means to define and specify AF in a uniform manner and develops a core ontology for the description of architectures. An architecture description language (ADL) is any form of expression for use in archi-

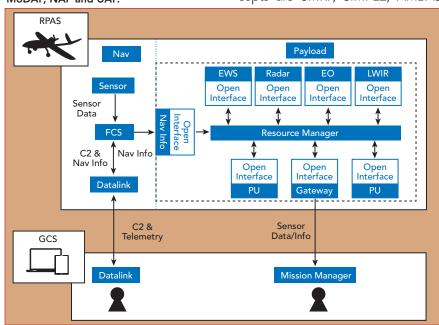


▲ Fig. 3 Relationship between DoDAF, MoDAF, NAF and UAF.

tecture descriptions. More recently, "wide-spectrum" ADLs have been developed which support a wider range of concerns like AADL, UML, BPMN, SysML or ArchiMate.

The Unified Modelling Language (UML) is a graphical language for visualizing, specifying, constructing and documenting the artifacts of a software-intensive system. It includes conceptual things such as business processes and system functions as well as concrete things such as programming language statements, database schemas and reusable software components.

There is a need to define and agree on an OTF to establish the common grounds for cooperation. The understanding and embracement of these concepts by all the involved communities is strongly required, at least from a high-level perspective. Stakeholders include those organizing and selecting research programs and projects together with the experts from Armed Forces and Procurement Organizations. should normally be done through incremental approaches. The complexity of these methodologies is in contrast with their aim to ensure an unambiguous common understanding. The frameworks selected should be as simple and clear as possible only ensuring the coverage of the needs they are supposed to resolve. EDA projects related to these concepts are SMRF, SIMPLE, AMBAS-



▲ Fig. 4 Architecture of the System.

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AN EXAMPLE OF IMOSA—
THE EORF PROJECT:
"ARCHITECTURES FOR
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ONBOARD RPAS PLATFORMS"

EORF⁹ was launched to explore the feasibility to define the IMOSA concept to achieve interoperability within payloads for small and medium RPAS (NATO class I and II). The BB defined, could be analysed and implemented in successive projects.

System advantages included the maximization of sensor data fusion performance, enhancing the RPAS capabilities in hostile environments and the improvement of the payload sensors interoperability and integration together with higher reliability, flexibility and lower product life-cycle costs for both manufacturers and final users.

Standards are essential to ensure adequacy of technical interface definitions, to allow comparisons and interoperability across vendors and systems and to create a shared competitive ecosystem. Examples of related standards are STANAG 4586 Unmanned Control System (UCS) UAV interoperability or STANAG 4626 covering modular and open avionics for architectures.

This would accommodate different payload configurations on the basis of combinations of sensors and weapons when needed; each one specifically designed in accordance with the intended results of the mission. *Table 1* shows the list of the most common and currently available sensors for RPAS applications.

After the analysis of the existent frameworks and methodologies, TOGAF¹⁰ was selected as being an open framework specialized in Systems/Enterprise architectures being the best one fitting the requirements of the project. TOGAF needs to be complemented with another framework aimed at vertical business domains and horizontal technology or specific application areas. NAF was chosen for that purpose.

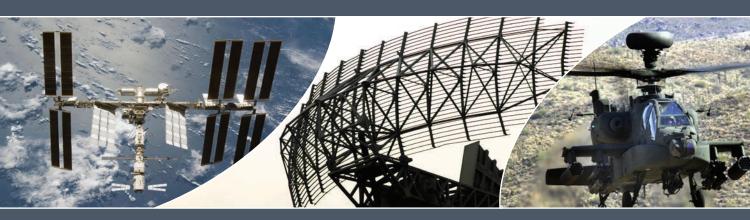
The EORF architecture is shown in Figure 4. The conceptualization of the BB is key in the definition of the target system architecture in order to make it modular and scalable. A certain combination of BB will be arranged for each mission/scenario. Consequently, "swapability," understood as the possibility to use different kinds of sensors under the same interface, is needed. The BB have been divided into four different categories according to TOGAF: business, data, application and technology. As these four categories cannot be described in this article only the technology view is shown. Its aim is to define the interfaces and standards to be used at physical and logical level.

NAF NSV-2b (System to System Port connectivity) is shown in *Figure* 5. It describes the communication protocol and the physical port specification of each port on the system, having all BB in the IMOSA the same communication and power unit protocol. Two possible implementations have been proposed, one based on Ethernet and another based on RapidlO as shown in *Table 2*.



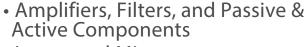


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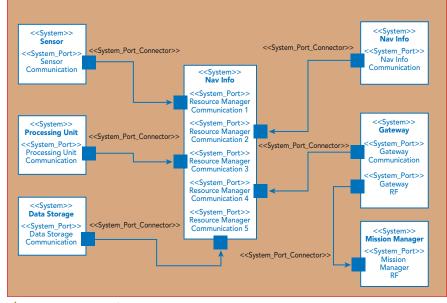
THE NEED TO PROMOTE AND USE MBSE FOR COLLABORATIVE PROGRAMMES

MBSE is a SE paradigm that emphasizes the application of rigorous visual modelling principles and best practices to SE activities throughout the System Development Life Cycle (SDLC).¹¹ New Defence Systems require iterative processes for development in a way that incremental verification has to be applied during design. Given the cost and scale of

investment to create a system, the life-cycle is becoming increasingly important affecting the operation and standards to create the product and the distribution of responsibilities amongst many defence contractors. The product acquisition life-cycle has to be tackled at all stages to properly cover all the needs of the stakeholders, so these methodologies have to be taken into account as of the pure research phase.

The production process needs to include Through Life Cost (TLC)

| TABLE 1 | | | | | |
|-------------|--|---|--|--|--|
| | SENSORS FOR RPAS APPLICATIONS | | | | |
| Sensors | Modes of use | | | | |
| Optical | Infra-Red (IR) Sensor- IR | Colour/Monochrome Daylight Electro-Optical TV- EO | | | |
| | Image-Intensified TV- IITV | Passive Night Optics- NVD | | | |
| Radar | Multi-mode Maritime Surveillance Radar- MSR | Ground/Dismount Moving Target Indicator- GMTI/DMTI | | | |
| | Synthetic Aperture Radar- SAR | Air-to-Air | | | |
| Laser | Laser Rangefinder- LR | Laser Imaging Detection and Ranging- LIDAR | | | |
| | Laser Target Designator- LTD | | | | |
| RF Signals | Intelligence of Communications System-COMINT | Electronic Support Measures- ESM | | | |
| | Electronic Intelligence System- ELINT | Electronic Counter Measures- ECM | | | |
| | Automatic Identification System- AIS | Air/Ground Data Link- A/GDL | | | |
| Others | Chemical, Biological, Radiological & Nuclear Weapons Detector-CBRN | | | | |
| Less Mature | Target Location Accuracy- TLA | Foliage Penetration FP in 2D or 3D | | | |
| Sensors | Detect And Avoid Radar- DAAR | Electronic Sensing & Effects- ESE | | | |
| | Infra-Red Search & Tracking for RPAS-IRST | Material/Ground Penetrating Radar- M/GPR | | | |

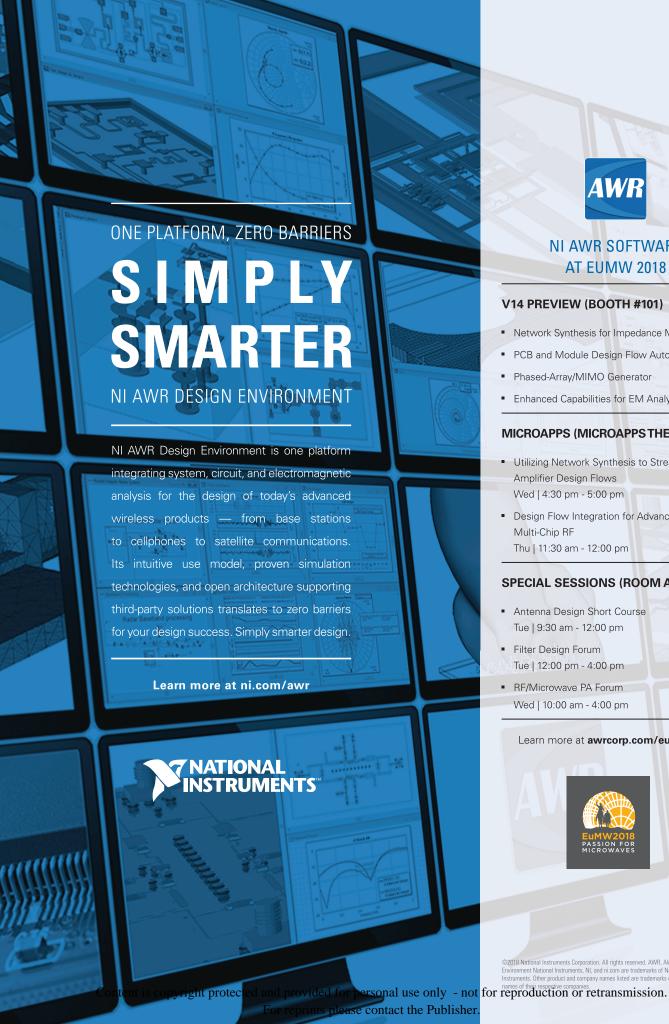


★ Fig. 5 NAF NSV-2b (System to System Port connectivity).

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with all maintenance, disposal and training costs in addition to the cost of creating the product. MBSE as software-based data exchange methodology with extensive and traceable validation and verifications strategies is essential to ensure that the product fulfils the customer requirements. Apart of the entire design and development process, a modelling of the system should be used throughout the lifecycle considering simple models of the design parameters and how information is passed and maintained throughout the design and development stages.

This methodology facilitates both to provide feedback to the customer and to support the work of multiple partners upon the same material. AMBASSADOR, 12 a project of the European Defence Agency, predicted reductions in costs and time using MBSE by about a third and the decrease of associated risks in development cost and schedule by about two thirds which would suppose an impressive advantage.

CONCLUSIONS & RECOMMENDATIONS

Defence Capabilities and Technology Research in the EU require an overarching effort to structure

and coordinate the several and different collaborative initiatives from a technical perspective to facilitate interoperability and ensure a successful outcome. From the author's experience, a commonly agreed OTF including SE/AF and Simulation frameworks with common methodologies and tools would facilitate the cooperative work and improve interoperability. Among the methodologies to be used, MBSE is extremely powerful for cooperation and to de-risk the whole capability development supporting verification and validation. Through the use of IMOSA and MBSE, research could be linked to capability development and very complex systems and systems of systems could be tackled, covering the TLC from a comprehensive perspective that could pave the way to future European Defence Capabilities. ■

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TABLE 2EXAMPLE OF IMPLEMENTATION BASED ON ETHERNET OR RAPIDIO

| | | Ethernet-based example | | RapidIO-based example | |
|--------------|-----------------------|---|----------------------------|---|--------------------------|
| | | «System_Port» Communication | «System_Port» RF | «System_Port» Communication | «System_Port» RF |
| Logical | Application Layer | ✓Encapsulation* ✓Encryption (AES-256) | ✓Encryption (AES-256) | ✓Encapsulation* ✓Encryption (AES-256) | ✓Encryption (AES-256) |
| | Middleware Layer | √ROS | √ROS | ✓JAUS over DDS (ARP6227) | ✓JAUS over DDS (ARP6227) |
| | Network Layer | ✓TCP/IP-MAC ✓UDP/IP-MAC | ✓TCP/IP-MAC ✓UDP/IP-MAC | √RapidIO | √RapidIO |
| Physical | Electronical Layer | ✓1000 Base-T(GigEthernet) | √RF @ 2, 4 GHz | √XAUI √OIF CEI | ✓RF @ 2, 4 GHz |
| | Mechanical Layer | √8P8C (RJ-45) √Circular MIL connector | √SMA-F | ✓LP-LVDS ✓LP-Serial | ✓SMA-F |
| | | «System_Port» Power Unit | | «System_Port» Power Unit | |
| Connector | | √8P8C (RJ-45) √Circular MIL connector | | ✓LP-LVDS | |
| Power Supply | | √+3.3, +5, +12, +24, +48 VDC | | ✓+3.3, +5, +12, +24, +48 VDC | |

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| OCTAVE BAND LOW NOISE AMPLIFIERS | | | | | | | | | |
|---|--|---|---|---|---|---|--|--|--|
| Model No. CA01-2110 CA12-2110 CA24-2111 CA48-2111 CA812-3111 CA1218-4111 CA1826-2110 | Freq (GHz) 0.5-1.0 1.0-2.0 2.0-4.0 4.0-8.0 8.0-12.0 12.0-18.0 18.0-26.5 | Gain (dB) MIN 28 30 29 29 27 27 25 32 | | +10 MIN +10 MIN +10 MIN | 3rd Order ICP +20 dBm +20 dBm +20 dBm +20 dBm +20 dBm +20 dBm +20 dBm | VSWR 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 | | | |
| | | | D MEDIÚM POV | | | | | | |
| CA01-2111 CA01-2113 CA12-3117 CA23-3111 CA23-3116 CA34-2110 CA78-4110 CA910-3110 CA1315-3110 CA12-3114 CA34-6116 CA56-5114 CA812-6115 CA812-6116 | 5.9 - 6.4 8.0 - 12.0 8.0 - 12.0 12.2 - 13.25 | 30 30 30 30 28 | 0.7 MAX, 0.5 TYP 1.0 MAX, 0.5 TYP 1.0 MAX, 0.5 TYP 1.2 MAX, 1.0 TYP 1.4 MAX, 1.2 TYP 1.6 MAX, 1.4 TYP 4.0 MAX, 3.0 TYP 4.5 MAX, 3.5 TYP 5.0 MAX, 4.0 TYP 5.0 MAX, 4.0 TYP 6.0 MAX, 5.5 TYP | +10 MIN +10 MIN +10 MIN +10 MIN +10 MIN +10 MIN +10 MIN +10 MIN +10 MIN +33 MIN +33 MIN +33 MIN +33 MIN +33 MIN +33 MIN | +20 dBm +20 dBm +20 dBm +20 dBm +21 dBm +41 dBm +43 dBm +40 dBm +40 dBm +41 dBm +41 dBm | 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 | | | |
| CA1415-7110 | 14.0 - 15.0 | 30 25 | 5.0 MAX, 4.0 TYP 3.5 MAX, 2.8 TYP | +30 MIN +21 MIN | +40 dBm +31 dBm | 2.0:1 | | | |
| CA1722-4110 | 17.0 - 22.0 | | CTAVE BAND AN | | +31 UDIII | 2.0.1 | | | |
| Model No. CA0102:3111 CA0106:3111 CA0108:3110 CA0108:4112 CA02:3112 CA26:4114 CA26:4114 CA618:4112 CA618:4116 CA218:4116 CA218:4110 CA218:4110 CA218:4110 CA018:4110 | Freq (GHz) 0.1-2.0 0.1-6.0 0.1-8.0 0.1-8.0 0.5-2.0 2.0-6.0 6.0-18.0 2.0-18.0 2.0-18.0 2.0-18.0 4.0-18.0 4.0-18.0 5.0-18.0 4.0-18.0 | Gain (dB) MIN 28 28 26 32 36 26 22 25 35 30 30 29 | 1.6 Max, 1.2 TYP 1.9 Max, 1.5 TYP 2.2 Max, 1.8 TYP 3.0 MAX, 1.8 TYP 4.5 MAX, 2.5 TYP 2.0 MAX, 3.5 TYP 5.0 MAX, 3.5 TYP 5.0 MAX, 3.5 TYP 5.0 MAX, 3.5 TYP 3.5 MAX, 2.8 TYP 5.0 MAX, 3.5 TYP 5.0 MAX, 3.5 TYP 6.0 MAX, 3.5 TYP | Power-out @ P1-dB +10 MIN +10 MIN +10 MIN +10 MIN +22 MIN +30 MIN +30 MIN +30 MIN +30 MIN +30 MIN +23 MIN +10 MIN +24 MIN +24 MIN | +20 dBm +20 dBm +20 dBm +32 dBm +40 dBm +20 dBm +33 dBm +30 dBm +30 dBm +31 dBm +31 dBm | VSWR 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 VSWR | | | |
| CLA24-4001 | 2.0 - 4.0 | -28 to +10 d | Bm +7 to +1 | 1 dBm +/ | /- 1.5 MAX | 2.0:1 | | | |
| CLA26-8001 CLA712-5001 CLA618-1201 AMPLIFIERS V | 2.0 - 6.0 7.0 - 12.4 6.0 - 18.0 WITH INTEGR | -28 to +10 d -50 to +20 d -21 to +10 d -50 to +20 d ATED GAIN | Bm +14 to +1 ATTENUATION | 9 dBm +/ | | 2.0:1 2.0:1 2.0:1 | | | |
| Model No. | Freq (GHz) | Gain (dB) MIN | Noise Figure (dB) Pow | | | VSWR | | | |
| CA001-2511A CA05-3110A CA56-3110A CA612-4110A CA1315-4110A CA1518-4110A LOW FREQUE | 0.5-5.5 5.85-6.425 6.0-12.0 13.75-15.4 15.0-18.0 | 23 28 24 25 30 | 2.5 MAX, 1.5 TYP 2.5 MAX, 1.5 TYP 2.5 MAX, 1.5 TYP 2.2 MAX, 1.6 TYP | +18 MIN +16 MIN +12 MIN +16 MIN | 30 dB MIN 20 dB MIN 22 dB MIN 15 dB MIN 20 dB MIN 20 dB MIN | 2.0:1 2.0:1 1.8:1 1.9:1 1.8:1 1.85:1 | | | |
| Model No. | Freg (GHz) (| Gain (dB) MIN | | | 3rd Order ICP | VSWR | | | |
| CA001-2110 CA001-2211 CA001-2215 CA001-3113 CA002-3114 CA003-3116 CA004-3112 | 0.01-0.10 0.04-0.15 0.04-0.15 0.01-1.0 0.01-2.0 0.01-3.0 0.01-4.0 | 18 24 23 28 27 18 32 | 4.0 MAX, 2.2 TYP 3.5 MAX, 2.2 TYP 4.0 MAX, 2.2 TYP 4.0 MAX, 2.8 TYP 4.0 MAX, 2.8 TYP 4.0 MAX, 2.8 TYP 4.0 MAX, 2.8 TYP | +10 MIN +13 MIN +23 MIN +17 MIN +20 MIN +25 MIN +15 MIN | +20 dBm +23 dBm +33 dBm +27 dBm +30 dBm +35 dBm +25 dBm | 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 2.0:1 | | | |
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DefenseNews

Cliff Drubin, Associate Technical Editor

Miniature Hit-to-Kill Interceptor Matures to Development Stage

he U.S. Army Cruise Missile Defense Systems Project Office awarded Lockheed Martin (LM) a \$2.6 million dollar contract to mature the Miniature Hit-to-Kill (MHTK) interceptor, evaluate its effectiveness and demonstrate manufacturing readiness as part of the Extended Mission Area Missile Program. Announced by the company at the Eurosatory exhibition, this award marks the MHTK's transition from the Science and Technology (S&T) phase to the Development phase.

Previous S&T contracts with the U.S. Army, together with LM investment, helped mature the MHTK missile from basic research to a concept demonstration with

HTK Interceptor (Source: Lockheed Martin Corp.)

two configurations to drive affordability.

two configurations—a semiactive RF seeker and an active RF seeker. MHTK has conducted a dozen flight tests with a combination of investment and contract funds. The most recent controlled flight test in January at White Sands Missile Range, N.M., demonstrated the interceptor's increased agility and validated performance of the airframe and electronics, which are now common between MHTK's

The MHTK missile is designed to defeat rocket, artillery and mortar targets through body-to-body contact without a warhead at ranges projected to exceed those of current and interim systems. The missile is just under two and a half feet in length, an inch and a half in diameter and weighs about five pounds at launch. The compact size allows multiple rounds to be packaged in a very small footprint to effectively combat complex threat situations like saturation attacks. The MHTK interceptor complements the LM family of Hit-to-Kill missile interceptors by delivering close range lethality with proven success for truly layered defense.

Bringing Autonomous Technology to the Battlefield

he U.S. Army Tank Automotive Research, Development and Engineering Center (TARDEC) awarded Oshkosh a \$49 million contract to integrate existing Palletized Load System (PLS) vehicles with scalable autonomous technology as part of the U.S. Army's Expedient Leader Follower (ExLF) program.

The ExLF program addresses the needs of the Leader Follower Directed Requirement and Program of Record by removing soldiers from the vehicle while operating in highly-contested areas. Oshkosh autonomous technology was designed with the flexibility to be operated in a variety of modes, including leader-follower, fully autonomous and teleoperation, to support manned or unmanned operations.

"The PLS has been an integral part of the U.S. Army's resupply and distribution fleet for over 25 years," said Pat Williams, VP and GM of Army and Marine Corps programs for Oshkosh Defense. "By equipping these vehicles with autonomous capabilities, we can significantly reduce our soldiers' exposure to enemy threats by taking them out of the vehicle altogether."

Under the contract, Oshkosh will integrate an initial 70 autonomy kits for Program Development and Operational Technical Demonstrations (OTD). The contract holds an option to procure up to 150 autonomy kits.



LVSR (Source: Oshkosh Corp.)

Building the Future, One RoboBoat at a Time

eams of students representing 13 schools from six different countries tested their engineering skills by developing autonomous boats during the recent 11th annual International RoboBoat Competition in Daytona Beach, Fla.

Sponsored by the Office of Naval Research (ONR) and the AUVSI Foundation, RoboBoat is an annual robotics contest where the next generation of engineers puts autonomous surface vehicles (ASV) through a series of advanced, water-based challenges that mirror real-world maritime operations.

"The challenges might seem simplistic, but before the boats even make it to the water to try and complete the course, there's a lot of complex engineering that goes into the ASVs' development," said Kelly Cooper, a program officer in ONR's Ship Systems and Engineering Research Division and a RoboBoat judge. "This competition really showcases the technical ingenuity of the students."

According to the recently-released DoN Strategic Roadmap for Unmanned Systems (short version), the goal is to "transform modern warfare" by seamlessly

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integrating unmanned systems into the naval services and across all domains. This is something ONR is already doing-pushing the path forward for autonomous technologies like swarming boats, aerial vehicles and unmanned surface ships and helicopters.

"RoboBoat showcases the talents of future engineers and serves as a basic introduction to some of what the Navy needs its autonomous systems to do," said Cooper. "We know there will be a strong pull from the commercial sector to have these kids come work for them, but we want the participants to know that the future is bright with the naval services as well. We have the jobs and we need their talent, too."

As in the past, this year's teams were largely composed of university students and were evaluated on their vessel design and performance. The design component focused on innovation, quality of engineering and craftsmanship. The performance component tested a vehicle's ability to execute specific missions on the water without any human interaction. As part of the performance challenge, the ASVs had to demonstrate their speed and navigation capabilities by passing through a set of gates before competing for any mission challenge points.

The mission tasks demonstrated the maritime systems' autonomous behavior in different scenarios, in-



RoboBoat (Source: U.S. Navy Photo)

cluding: speed; automated docking, which demonstrated the ability to launch and communicate with an aerial drone; finding a path in a crowded area; target identification; precise navigation; and, finally, return to dock.

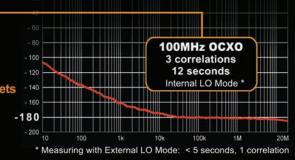
Institut Teknologi Sepuluh Nopember (Indonesia) was this year's biggest winner, bringing home the top prize of \$6,000. Georgia Institute of Technology won second prize and \$5,000; Hagerty High School (Florida) took third and \$3,000; and Embry-Riddle Aeronautical University (Florida) came in fourth, earning \$2,000.

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France, U.K. Regulators Position for 5G

egulators in France and the U.K. are taking steps to enable the deployment of 5G services in their respective countries.

In France, the government released a roadmap for 5G, articulating several goals: launching pilot projects in several regions, hosting "pioneer" industrial applications, allocating new spectrum and ensuring the commercial rollout in at least one major city by 2020 and coverage of the main transport routes by 2025. To accomplish these goals, the country's telecommunications regulator Arcep has identified four steps, including allocating spectrum, launching pilot projects in 2019 and streamlining 5G rollout.

For sub-6 GHz coverage, Arcep plans to allocate 3.4 to 3.8 GHz and move existing users to other bands. For higher data rates, the 26.5 to 27.5 GHz band has been identified, which is consistent with European efforts to establish a standard mmWave band for 5G. Arcep is also considering using 1.5 GHz, planning to explore the feasibility beginning this summer.

5G pilot projects are being planned or have been launched in 11 French communities, and 11 new trials were recently announced, including three connected vehicle use cases. Arcep is open to expanding the number of trials in France, the only limitation being available frequencies in the region.

Arcep's "5G Work Programme" is available to download from the agency's website: www.arcep.fr.

Across the Channel, Ofcom published a report defining the U.K.'s five-year plan for spectrum to meet the demands of fixed wireless links, such as backhaul for mobile base stations, "last mile" broadband services, TV program distribution from studio to transmitter, emergency services and private networks. The report follows a process of consulting with stakeholders to identify existing and emerging needs for spectrum. Ofcom identified secular and technology trends during the study, including:

- 5G will require greater bandwidth, both for services to users and the backhaul to support them.
- Financial services firms are using direct wireless links to minimize latency, a differentiator in financial transactions.
- There's increasing interest in the spectrum at 60 GHz, for new use cases, and above 92 GHz, for high capacity backhaul networks.

The Ofcom study evaluated frequency uses and projected needs below 20 GHz, between 20 and 45 GHz and above 45 GHz. The most urgent needs identified are above 45 GHz, prompting Ofcom to take "immediate steps" to allocate new spectrum from 66 to 71 GHz to support new 5G use cases and make the 57 to 71 GHz band "license exempt," to allow rapid deployment.

The Ofcom report can be downloaded from the agency's website: www.ofcom.org.uk.

Asia to Lead 5G Subscribers by 2025

ith initial 5G standards now finalized by the 3GPP, mobile operators are deploying infrastructure to prepare for the availability of mobile devices and other user equipment in 2019. GSMA, the mobile industry's trade group, estimates the Asia-Pacific region will lead the world with 5G connections by 2025—some 675 million, which will be more than half of the world's 5G connections. China, South Korea, Japan and Australia will drive the region's growth.

Despite the buzz, 5G will not replace LTE, which will continue to grow, as it is adopted in emerging markets such as India, Indonesia, Thailand and Vietnam. In 2017, LTE surpassed 2G to become the leading mobile technology in the region and, by 2025, GSMA estimates 62 percent of Asia's mobile connections will be on LTE, compared to 14 percent on 5G.

With China and India, the two largest mobile markets, the Asia-Pacific region is home to more than half of the world's mobile subscribers. The number of unique mobile subscribers in the region is estimated to have been 2.7 billion at the end of 2017 and is forecast to grow by 424 million to 3.2 billion in 2025. Almost half of the new subscribers will be in India, nearly 3× the new subscribers in China.

GSMA's analysis and forecast for the Asia-Pacific region are contained in a recently published report, "The Mobile Economy: Asia-Pacific 2018," which is available from the GSMA website at www.gsma.com/mobileeconomy/asiapacific.

Handsets Drive WIN Semi's Growth

aiwan-based WIN Semiconductors, the world's largest GaAs foundry, reported strong second quarter and first half revenue growth driven by the handset market. However, the company said inventory corrections across all markets will cause third quarter revenue to decline around 10 percent compared to the second quarter.

Second quarter net revenue was NT\$4,567 million (approximately \$149 million), 20 percent above the prior year's quarter and 2 percent above the first quarter. First half revenue was NT\$9,031 million (\$295 million), 27 percent above the prior year period, as MMICs for smartphones grew by double-digits. WIN said approximately 35 to 40 percent of second quarter revenue was from the cellular market, 25 to 30 percent from Wi-Fi, 15 to 20 percent from infrastructure and approximately 16 percent from other markets.

To complement RF/microwave applications, WIN has been developing optoelectronic process technol-

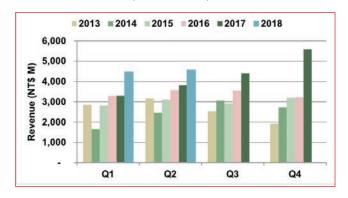
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ogy to fabricate photodiodes and laser diodes for the growing 3D sensing market.

WIN reported second quarter gross margin of 32.4 percent, down from 34.1 percent in the first quarter, and operating margin of 20.7 percent, compared to 23.3 percent in the first quarter. The company attributed the declines to product mix. Net income increased almost 24 percent sequentially and year-overyear, which WIN said reflected the favorable foreign exchange rate with the U.S. earnings per share (EPS) was NT\$2.16, compared to NT\$1.74 in the first quarter and NT\$1.85 in the prior year's quarter.



LTE via Balloon Over Kenya

elekom Kenya and Loon, an independent business unit of Alphabet, have signed an agreement to use Loon's high altitude balloons to provide LTE service to rural regions of Kenya. The agreement with Telekom Kenya will be Loon's first in Africa, beginning in 2019 with a pilot over central Kenya, which has limited service because of the mountainous terrain.

Using balloons avoids the cost of installing terrestrial infrastructure in areas of low population density, and the balloons fly well above aircraft and weather—in the stratosphere at 60,000 feet. The balloons carry solar-powered base stations that send and receive LTE signals to users on the ground. Backhaul to the service provider is accomplished via a relay network among the balloons.

In 2017, Loon demonstrated its capability with Telefonica, providing internet connectivity to tens of thousands of people in Peru who were displaced by extreme rains and flooding. Loon also worked with AT&T and T-Mobile to connect more than 100,000 people in Puerto Rico after the island was ravaged by Hurricane Maria.



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CommercialMarket

Cliff Drubin, Associate Technical Editor

NB-IoT, CAT-M, SIGFOX and LoRa Battle for LPWA Network Dominance

ellular and non-cellular LPWA network connections will grow globally at a 53 percent CAGR until 2023, driven by market growth in smart meters and asset trackers, according to a new report from ABI Research. In 2017, smart meters and asset trackers contributed to almost three-quarters of all LPWA network connections, dominated by non-cellular LPWA network technologies. However, by 2023, non-cellular LPWA will cede its market share dominance to NB-IoT and LTE-M, as cellular LPWA moves to capture over 55 percent of LPWA connections. Regionally, although Western Europe and North America witnessed early deployments of public LPWA networks, the Asia-Pacific, especially China, has been a pivotal market for driving large-scale adoption of NB-IoT and LoRa.

"LPWA network technologies are making it feasible to build simple, small and low-cost footprint devices

Drives global LPWA network connections to pass 1B by 2023

that can track and monitor everything from seafreight containers to bicycles, patients to pets, supermarket trolleys to pallets, paving the way

for new innovative solutions and business opportunities," says Adarsh Krishnan, principal analyst, ABI Research. Asset tracking, which includes tracking stationary or slow-moving assets, will have the largest share of LPWA connections in 2023, accounting for over 45 percent worldwide.

Smart meters deployed by energy and water utilities will be the second largest vertical IoT application in 2023, contributing over one-third of the global LPWA device connections. Early adoption from meter vendors such as Sensus, Itron, Kamstrup, Arad and Holley metering means that non-cellular LPWA technologies are well positioned to capture two-thirds of the LPWA connections in smart meters by 2023.

In 2017, SIGFOX had the largest share of public LPWA connections worldwide benefiting from its first mover advantage in Europe. "SIGFOX has continued to stay a step ahead in public LPWA networks with the rollout of the Monarch cognitive network service in early 2018. The Monarch service enables SIGFOX devices to automatically adapt to RF changes allowing for seamless roaming across SIGFOX networks," Krishnan explained. Louis Vuitton's Echo travel bag tracker was the first commercial SIGFOX device to leverage the Monarch service in over 100 airports across 26 countries. In contrast, LoRa gained significant market share as a popular connectivity technology for private networks, witnessing over 54 percent year-on-year growth in 2017.

Private LPWA networks, built to address a single vertical application or an individual enterprise, have been a popular choice for over a decade and accounted for 93 percent of LPWA connections in 2017. LoRa and other non-cellular LPWA technologies have benefited from the decreasing cost of ICs, low implementation costs and flexibility of private networks that can be tailored to meet specific enterprise IoT applications. LoRa has witnessed exponential growth in APAC, especially in China where ZTE has deployed China LoRa Application Alliance (CLAA) LoRa networks in 40 cities and is starting to ramp up deployment of smart meters, parking sensors, air-quality monitoring sensors and other smart city solutions. However, as the geographic footprint of public networks rapidly expands, cellular and non-cellular public networks will capture over 70 percent of LPWA connections by 2023.

80M Smart Home Thermostats Linked to Smart City Grid Control by 2022

he growing power of smart home devices and services will increasingly extend their influence outside of the home and into wider smart city programs, finds ABI Research. Over the next five years, smart home and smart city providers will increasingly leverage the overlap between these two traditionally separate markets as smart home services provide a ready and expandable Smart City IoT resource.

"So far, smart city programs have been dominated by broad, large-scale implementations. Either these projects will expand to embrace smart home partners or they will see some of the primary applications encroached upon by progressive smart home providers," says Jonathan Collins, research director, ABI Research.

By 2022, a global install base of nearly 300 million smart homes will put smart home providers in the position to provide a ready data source for smart city applications. Current smart city projects typically address applications including transportation, healthcare provision, environmental management and more. Increasingly, smart home providers are showing they can deliver similar functionality by adding additional application capabilities for their smart home customer base.

Perhaps the best current example of smart home deployments engaged in driving smart city benefits is the integration of smart thermostats into utility demand management programs. Instead of utilities developing their own direct to consumer smart home plays, they have instead turned to smart home players such as Nest, Honeywell and others to deliver the remote control over end-user heating and cooling demands to help manage peak loads. ABI Research finds that worldwide by 2022, more than 80 million homes with smart thermostats are set to have control of the heating and cooling in the home linked to smart grid control.

Already home security smart home players Vivint

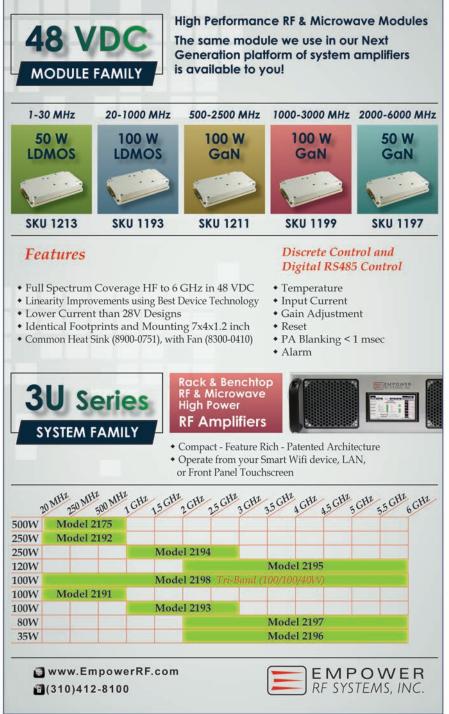
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and Ring (now part of Amazon) are providing video surveillance features using external smart home cameras. Vivint's Streety app provides shared video access to subscribers within a fixed neighborhood, replicating smart city video monitoring of public spaces but through a crowdsourced model. Other applications are still in their earliest stages. Parking manage-

ment is an often-tackled smart city application, but the rise of crowd-sourced parking solutions presents another smart home opportunity. Although still in its earliest days, the potential for crowdsourced parking services to be integrated into wider smart home management features such as access control or electric vehicle charging could prove compelling integration drivers.



5G Not Enough for Mobile Service Providers to Enter Smart Manufacturing

espite high ambitions for the smart manufacturing sector, mobile service providers (MSP) are currently secondary players in this market. Consequently, their short-term opportunity in manufacturing is forecasted to be only \$2.6 billion by 2022, according to ABI Research.

"The manufacturing market has grown without MSPs so far, and if they don't play their cards right, it will continue to do so," said Pablo Tomasi, senior analyst at ABI Research. "UnTelco—the need for MSPs to think and act beyond their traditional boundaries—in manufacturing is about entering a wellentrenched sector developing new market strategies and partnerships. MSPs have a chance to enter the smart manufacturing market building from the ground up, gaining trust as partners and proving that the value of their offering is beyond what is currently delivered in the market. 5G is a promise, but alone is not enough and with doubts on what business model will support it, 5G's ability to integrate with legacy technologies and the actual results delivered in harsh factory environments, there is much uncertainty about whether 5G will be a game-changer for MSPs in manufacturing."

Partnering with market leaders will be essential—the recently announced partnership between Orange and Siemens is an example of what should be a growing trend. 5G will not be in the factory for a few years, and to be successful, a wider alignment between industrial vendors and MSPs is essential. Even the private LTE solutions currently available are only at a very early stage in manufacturing and still lack the success stories needed to prove their value in the market.

"The manufacturing market looks for enhancements, not disruption, and for solutions, not technologies. MSPs should tailor their offerings, including 5G, to these enhancements and solutions," Tomasi concluded.

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MERGERS & ACQUISITIONS

Carlisle Interconnect Technologies announced the purchase of Tenencia Ltd. Tenencia is an EASA Part 21 Design and Production organization based in Coventry, U.K. Tenencia operates under AS9100 and carries CAA part 21 production approval and is approved to both AS9100D and BS EN ISO 9001:2008. Tenencia specializes in the integration and certification of electrical/avionics systems, cabin systems, internal and external structure, VIP interiors and commercial aerospace applications on a wide range of aircraft. In acquiring Tenencia, CarlisleIT broadens its global capabilities for design certification of commercial aircraft to both EASA and FAA design and production requirements.

Baylin Technologies Inc. announced that it has entered into a share purchase agreement to acquire all of the issued and outstanding shares of Alga Microwave Inc. for total consideration of \$27 million, consisting of up-front cash consideration of \$21 million, \$4 million in Baylin shares and \$2 million in deferred consideration, as well as a related agreement to purchase Alga's operational facilities in Kirkland, Quebec. Baylin is to purchase all of the outstanding shares of Alga, through a newly incorporated subsidiary, for up-front consideration of \$25 million, subject to customary adjustments.

COLLABORATIONS

Keysight Technologies Inc. announced that the company is extending its collaboration with **UNISOC Inc.** to participate in the CMCC 5G large-scale trials. Keysight is helping UNISOC accelerate 5G New Radio (NR) chipset development with substantial support from GTI. Both UNISOC and Keysight achieved 5G NR PHY layer interoperation based on the latest 3GPP Release 15 5G NR standards in the CMCC 5G Innovation Center Lab, and demonstrated this achievement at the 22nd GTI workshop. The event brought together mobile operators, vendors and companies from vertical industries to address and discuss key issues and the latest progress in 4G and 5G technology development.

AccelerComm has announced its 5G NR polar IP has been adopted by National Instruments (NI). The IP has been selected for use in NI's USRP RIO software defined radio family of products, which are used by wireless researchers in academic and industrial teams working across a range of mobile and communication technologies to accelerate product development. The USRP RIO uses 2 × 2 MIMO transceivers, each tunable to independent frequencies between 50 MHz to 6 GHz with 40 or 120 MHz per channel, giving a real-time bandwidth of 80 dB of dynamic range.

Planar Monolithics Industries Inc. (PMI) has signed an agreement with Pasternack Enterprises who will private-label a selection of PMI manufactured products under the Pasternack brand name. Through Pasternack, this selection of products will be available off-the-shelf for immediate shipping. This new partnership will provide customers with urgent RF product needs access to an extensive inventory of industry-leading components through Pasternack, along with Pasternack's 24/7 sales and technical support, online purchasing and same-day shipping.

Leti, Transdev and IRT Nanoelec announced a pilot program to characterize and assess LiDAR sensors to improve performance and safety of autonomous vehicles. In the pilot program, Leti teams will focus on perception requirements and challenges from a LiDAR system perspective and evaluate the sensors in real-world conditions. Vehicles will be exposed to objects with varying reflectivity, such as tires and street signs, as well as environmental conditions, such as weather, available light and fog. In addition to evaluating the sensors' performance, the project will produce a list of criteria and objective parameters by which various commercial LiDAR systems could be evaluated.

At Mobile World Congress Shanghai 2018, **China Unicom** and **Huawei** announced a 5G strategic partnership agreement, culminating in a signing ceremony at the Shanghai's Kerry Center. In a release issued by the companies, the two said, "Huawei and China Unicom will fully leverage their respective innovative strengths in 5G and focus on cooperation in E2E 5G technical verification, cooperation with vertical industry partners, building of the 5G ecosystem and 5G service incubation and promotion."

ACHIEVEMENTS

Custom MMIC announced their recognition by Raytheon Co., with an award in May during the Raytheon Integrated Defense Systems (IDS) 2018 Supplier Excellence Conference. Raytheon's annual Supplier Excellence Awards program recognizes suppliers who have provided outstanding service and partnership in exceeding customer requirements. Award candidates are judged on certain criteria, including overall quality, on-time delivery and demonstrated commitment to continuous improvement. A 5-Star recognition is the highest level of recognition a Raytheon IDS business supplier can achieve for excellence in quality and performance, and Custom MMIC was one of nine companies selected.

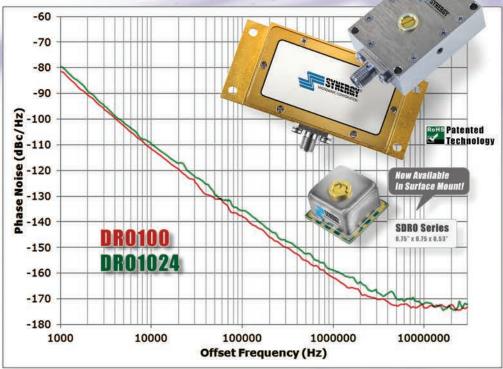
Orbital Research Ltd., a provider of high performance frequency conversion products for SATCOM industries, announced they have been certified under ISO 9001:2015 as of May 28.

BAW filter manufacturer **Akoustis Technologies** has completed the qualification of its first-generation XBAW wafer technology and the attendant single crys-

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| SDRO1024-8 | 10.240 | 1 - 15 | +8.0 @ 25 mA | -105 |
| SDRO1118-7 | 11.180 | 1 - 12 | +5.5 - +7.5 @ 25 mA | -104 |
| SDRO1121-7 | 11.217 | 1 - 12 | +5.5 - +7.5 @ 25 mA | -104 |
| SDRO1130-7 | 11.303 | 1 - 12 | +5.5 - +7.5 @ 25 mA | -104 |
| SDRO1134-7 | 11.340 | 1 - 12 | +5.5 - +7.5 @ 25 mA | -104 |
| SDRO1250-8 | 12.500 | 1 - 15 | +8.0 @ 25 mA | -105 |
| Connectorized Mode | els | | | |
| DRO80 | 8.000 | 1 - 15 | +7.0 - +10 @ 70 mA | -114 |
| DRO100 | 10.000 | 1 - 15 | +7.0 - +10 @ 70 mA | -111 |
| DRO1024 | 10.240 | 1 - 15 | +7.0 - +10 @ 70 mA | -109 |
| KDRO145-15-411M | 14.500 | * | +7.5 @ 60 mA | -100 |

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Around the Circuit

tal materials process at its Canandaigua, N.Y. wafer fab. The XBAW-1 (XB1) process is the industry's first single crystal BAW technology for the expanding RF filter market for 4G/LTE, 5G, Wi-Fi and military radar. The XB1 process supports applications from 1.5 to 7 GHz and provides wide bandwidth and high linearity. The process uses patented, single crystal piezoelectric materials and MEMS wafer manufacturing and is compatible with both conventional and flip-chip packaging.

Finnish telecommunications company Elisa has become the first operator in the world to begin commercial use of a 5G network and to start offering 5G subscriptions. The first person to use the 5G network was Finland's Minister of Transport and Communications, Anne Berner, when she made a video call to Kadri Simson, the Minister of Economic Affairs and Infrastructure in Estonia. The world's first commercial 5G networks have now been launched in the Finnish city of Tampere and Estonia's capital city Tallinn, and Elisa is also updating its network to be 5G-ready across Finland.

Raytheon IDS held a Supplier Excellence Conference and presented awards to recognize suppliers who have provided outstanding service and partnership in exceeding customer requirements. KMED (via its General Microwave facilities in Israel and New York) was one of 55 companies recognized by Raytheon's IDS business for 4-Star honors.



CONTRACTS

Harris Corp. has been awarded three multi-award IDIQ contracts with ceilings totaling \$1.5 billion to provide the National Geospatial-Intelligence Agency (NGA) with geospatial data services for up to 10 years. Harris will create, manage and disseminate high-quality geospatial-intelligence (GEOINT) information for use by the U.S. intelligence community and military worldwide under contracts that cover all three areas of NGA's JANUS program—geography, imagery and elevation.

Altamira Technologies Corp. has been awarded the Air Force Research Laboratory's (AFRL) \$24.6 million Distributed Radio Frequency Sensing (DRS) contract to provide next-generation RF sensing technologies through advanced R&D of RF systems and sub-systems. The five-year CPFF contract will support the development of innovative solutions applying DRS to contested and congested spectrum environments.

CACI International Inc. announced that it has been awarded a \$48 million task order to provide engineering and technical related services (ETRS) to the Naval Surface Warfare Center, Indian Head Explosive Ordnance Disposal Technology Division. The five-year, singleaward contract, awarded under the U.S. Navy's SeaPort II Omnibus Engineering and Technical Support Services contract vehicle, represents continuing engineering services work in CACI's surveillance and reconnaissance market area.

Teledyne Wireless, a business unit of the Teledyne Defense Electronics Group, has been awarded a \$4.4 million sole source contract from the Naval Supply Systems Command (NAVSUP) for maintenance and repair operations involving traveling wave tubes (TWT) utilized in AEGIS systems supporting SPY-1 Radar. Execution of the contract award will be performed at Teledyne's 160,000 square foot production facility in Rancho Cordova, Calif.

PEOPLE



▲ Paul J. Fego

Qorvo® announced the appointment of Paul J. Fego as corporate vice president, global operations, effective immediately. Fego will report to Bob Bruggeworth, president and CEO of Qorvo, and will assume responsibility for Qorvo's operations, including internal and ex-

ternal wafer fabrication, assembly and test technology and manufacturing. Fego most recently served as vice president and manager of the Worldwide Manufacturing Group at Texas Instruments, where he managed all of its wafer fabrication, assembly and test operations in nine countries.

Insulated Wire Inc. (IW) announced that, following the retirement of a French delegate, IW Microwave Products Division President John Morelli has been appointed as the secretary for IEC/SC46F, a subcommittee of IEC/ TC46. IEC/SC46F is responsible for RF and microwave connectors and components international standardization. Morelli, who is sponsored by IW, brings significant

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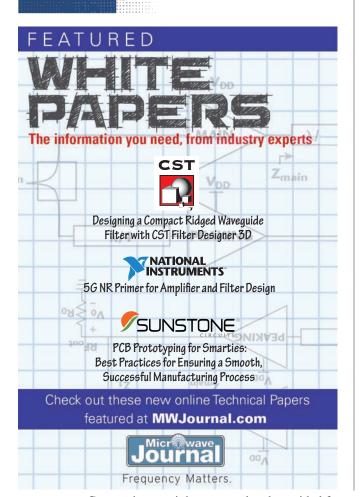
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Around the Circuit

RF and microwave connector and component experience to the position. Morelli had been serving as the chief technical advisor for the U.S. National Committee's Technical Advisory Group to IEC/SC46F.

REP APPOINTMENTS

RFE announced the appointment of the following regional manufacturer's sales representatives: WLM Components covering New England and Upstate New York and Radar Systems Technology covering international. RFE is an original design manufacturer (ODM) serving military, industrial and commercial markets with a product line of small profile, high performance converter and synthesizer sources.

RFMW Ltd. announced a distribution agreement with Integrated Device Technology (IDT) effective immediately. Under the agreement, RFMW is franchised for worldwide marketing and sales of IDT's portfolio of RF, microwave, mmWave and RF timing products. IDT offers high linearity RF components including modulators and demodulators, mixers, synthesizers, attenuators, switches, amplifiers and phase locked loops. RFMW is a specialized distributor providing customers and suppliers with focused distribution of RF and microwave components as well as specialized component-engineering support.

Richardson RFPD announced that it has entered into an expanded agreement with Maxwell Technologies Inc., a developer and manufacturer of capacitive energy storage and power delivery solutions. The new agreement builds on the long-term relationship between the two companies, and completes Richardson RFPD's global network by adding Europe, Japan and Korea to its ultracapacitor sales regions. For over 50 years, Maxwell's world-class research and product development teams have established the company as a global leader in developing, manufacturing and marketing energy storage and power delivery solutions for automotive, grid energy storage, wind and industrial applications.

W. L. Gore & Associates Inc. (Gore) announced that WireMasters is the first authorized distributor of select GORE® Space Cables for high data rate applications. Product offerings in stock at WireMasters include Type GBL (Balanced Shield Line) for dataline applications and Type SpaceWire for satellite, telescope observatories and other critical spaceflight operations. Headquartered in Columbia, Tenn., WireMasters is an industry leader in the sales and distribution of Mil-Spec BMS and EN wire, cable, tubing and accessories. They have provided best-in-class, value-added services to the aerospace and defense market for 30 years.



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Welcome to EuMW 2018: **Find Your Passion for** Microwaves in Madrid

Magdalena Salazar Palma and José Ignacio Alonso Montes General Co-Chairs EuMW 2018 Ivar Bazzy President, Horizon House Publications

> For complete coverage of the EuMW 2018 conference, event news, exhibitor product information and special reports from the editors of Microwave Journal, visit our online show daily at mwjournal.com/eumw2018

s part of the microwave industry, we all have a "Passion for Microwaves," which is the theme for this year's European Microwave Week (EuMW). The co-chairs and organizer of EuMW 2018 welcome you to Madrid, the economic and cultural centre of Spain and the third largest city in the European Union. This is the 21st EuMW, and takes place at IF-EMA Feria de Madrid from Sunday 23 to Friday 28 September. After the very successful 2017 event in Nuremberg, the EuMW comes to the lively, cosmopolitan and friendly city of Madrid. This conference event was started by the European Microwave Association (EuMA) in 1998, and is made up of the 48th European Microwave Conference (EuMC), taking place from 25 to 27 September, the 13th European Microwave Integrated Circuits Conference (EuMIC), taking place from 24 to 25 September, and the 15th European Radar Conference (EuRAD), running from 26 to 28 September. The three conferences are accompanied by the three-day trade show covering RF and microwave technology that attracts about 300 exhibitors and is the largest in Europe.

Over 430 reviewers and the 110 members of the Technical Program Committee selected an excellent program comprising of 521 presentations. The program also includes six special sessions. We are proud to host in particular the special session celebrating the 20th anniversary of EuMW, which encompasses presentations by our esteemed colleagues who launched this successful event as envisioned by a recently established EuMA back in 1998. Two other special sessions will highlight the research activities in Latin America and 5G technology in the Asia-Pacific Region. Two more special sessions present the latest research on additive manufacturing and high frequency flexible bendable electronics for wireless communication systems. Finally, a special session is devoted to radar projects at the European Defense Agency.

The regular program is organized in 87 oral sessions and five interactive sessions. The program is complemented by 33 workshops and eight short courses, covering the most relevant topics ranging from mmWave circuits to 5G, from power amplifiers to automotive radar and from THz technology to

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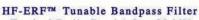
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SATCOM, from Sunday 23 to Friday 28 September.

This year's Defence, Security and Space Forum (DSS) is devoted to "Integrating Unmanned Aerial Vehicles (UAV) into Defence and Security Scenarios." The DSS Forum organizers have succeeded in attracting highlevel speakers to discuss the need from a defense and security perspec-

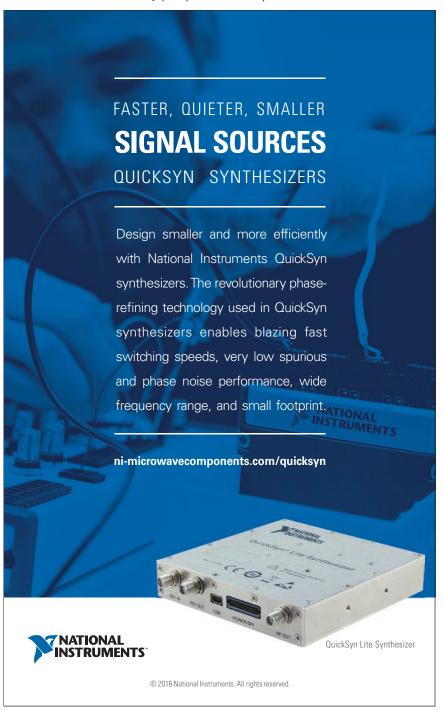
tive of integrating UAVs into current air traffic control and air defense systems, together with related technological challenges and solutions.

Internationally renowned speakers will discuss the latest trends and developments in their keynotes at the conferences' plenary sessions. At the opening session of the EuMW, Enrique Blanco, Telefónica Global

CTIO, will outline how the 5G technologies will impact future communication networks. The EuMIC opens with presentations by Chuck Campbell, engineering senior fellow with the Infrastructure and Defense Products Division of Qorvo, U.S., on the progress and problems of GaN MMIC design, and by Sebastián Gómez-Díaz, from University of California, Davis, U.S., on THz nanoplasmonics with 2D materials. Bill Deal, distinguished engineer in the RF and Mixed Signal Department of Northrop Grumman, U.S., will close the EuMIC with a review on THz transistors and their applications. During the EuRAD opening, which is held in conjunction with the DSS Forum, M. Carmen Barbero, head of Naval Radar Programs, Indra Sistemas, Spain, will present the new radar generation for the F-110 frigate integrated masts, and Stefano Pirandola, from York Centre for Quantum Technologies, U.K., will discuss quantum radar. Domingo Castro, Rafael Casado and Jacobo Martínez-Villa, from Indra Sistemas, Spain, will present the S3T Spanish ESA (European Space Agency) Radar facility for space debris at the EuRAD closing session. The EuMW will close with a presentation by Giuliano Gatti, space segment manager of ESA Galileo Satellite Navigation Program.

The traditional Women in Microwave Engineering (WiM) event, cosponsored by the IEEE MTT-Society, will focus on communications technology for space exploration, and both women and men are welcome. Attendees will visit one of the following two centers located near Madrid: the NASA-MDSCC (Madrid Deep Space Communications Complex) or the ESA-ESAC (European Space Astronomy Centre). Besides visiting the center, presentations will be given by scientists working at MDSCC or ESAC. As initiated during EuMW 2017, the WiM attendees will have the opportunity to interact with high school students who are invited to participate in this event. Early registration is encouraged, as the number of participants is limited.

EuMW 2018 will host several events especially for younger en-



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gineers. These include the very stimulating and successful Student Challenge, which will have the same format as in previous years. The Student Design Competition comprises two tasks to be prepared in advance. It will also feature a design task to be carried out on-site. This will take place in the form of a hands-on design experience event. The latter is

also part of the Student and the Doctoral School, which both start with a high-level, half-day lecture program. The Career Platform will continue the successful format of previous years. Finally, two sessions devoted to young professionals are offered.

The week would not be the "Week" without its traditional social events. These include Mon-

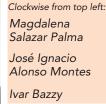
day's EuMIC Get-Together, which this year will be held at a beautiful restaurant located in the heart of Madrid's modern downtown, Tuesday's Welcome Reception, sponsored by Keysight Technologies, which will also be held off-site at the Palacio del Negralejo and the Eu-RAD Lunch on Friday. In addition, a private visit to the Thyssen-Bornemisza Museum, one of Madrid's Golden Triangle of Art, together with the Prado and the Reina Sofía national galleries, followed by a cocktail dinner, has been organized for Wednesday evening.

The Week's program will let you enjoy Europe's microwave event in 2018 and will give you plenty of opportunities to satisfy your professional "Passion for Microwaves." Do not forget to explore the friendly city of Madrid, where everyone feels at home. Madrid's rich artistic and natural heritage, cutting edge transport network, quality accommodation, fine cuisine and the passion locals show when enjoying their city's day and nightlife make it one of the most attractive cities in the world. If time permits, we invite you to visit some of the many nearby landmarks, from Alcalá de Henares, where Miguel de Cervantes, the well-known author of Don Quijote de la Mancha, was born 471 years ago, to Segovia, Toledo and more.



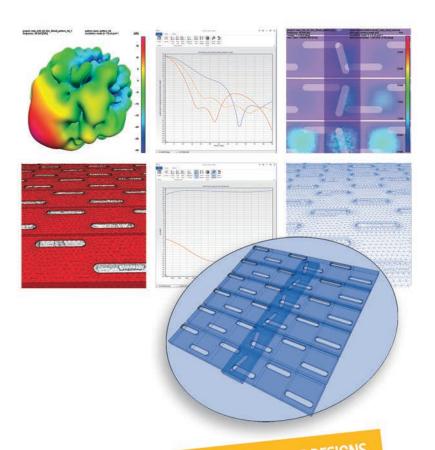








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Radio tower image courtesy of Tom Rauch, W8JI

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Attending European Microwave Week 2018

Compiled by Patrick Hindle Microwave Journal *Editor*

uropean Microwave Week (EuMW) 2018 is being held in the exciting city of Madrid, Spain for the first time ever. Bringing industry and academia together, EuMW is a six day event, including three cutting edge conferences, workshops and an energetic trade exhibition featuring leading players from across the globe. EuMW 2018 provides access to the very latest products, research and initiatives in the microwave sector. It also offers you the opportunity for face-to-face interaction with those driving the future of microwave technology.

CONFERENCES

The conference event is made up of the 48th European Microwave Conference taking place from 25 to 27 September, the 13th European Microwave Integrated Circuits Conference taking place from 24 to 25 September and the 15th European Radar Conference running from 26 to 28 September. The conferences encompass a wide range of topics including:

- Microwave, mmWave and sub-mmWave systems
- Antennas and propagation
- Wireless technologies
- Telecommunication (RF, microwave and optical)

- ICs, semiconductor materials and packaging
- Radar architectures, systems and subsystems
- Sensors and remote systems
- Test and measurement

European Microwave Conference (EuMC) 25-27 September

In its 48th year, the European Microwave Conference (EuMC) comes again to Spain, after 25 years. The last Spanish edition of the EuMC was held in Madrid in 1993, and in that time the flagship conference of the current EuMW was not associated to the European Radar Conference (EuRAD) and to the European Microwave Integrated Circuits Conference (EuMIC). In its present format, the EuMC is able to reach a wider audience, since its traditional and widespread set of covered topics (mainly focused on microwave and wireless components, systems and technologies) is enriched with radar technologies and microwave integrated circuits (in this edition through four joint sessions with EuMIC and nine with EuRAD).

The simultaneous celebration of the three conferences during the same week, plus the high number of technical workshops, short courses, associated events, as well as

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(Demos at EuMW booth #28A)

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the industry exhibition, will contribute to the continuous success that EuMW, and particularly EuMC, experiences yearly. The entire team of the EuMW 2018, and particularly the EuMC 2018 team, with the help of the Technical Program Committee members and paper reviewers, have done a great job in creating a coherent, balanced and complete program for this year's conference, with special emphasis on the latest trends in microwave, mmWave, THz and wireless technologies. In summary, 355 papers grouped in 51 technical sessions or presented in the four interactive forums, nine industrial session keynotes, 28 workshops and eight short courses have been accepted in the present edition of EuMC. Moreover, five special sessions will be held in the following selected domains: "20th Anniversary of the European Microwave Week," "Microwave Research in Latin America," "5G Technology in Asia-Pacific," "Additive Manufacturing" and "High Frequency Flexible Bendable Electronics for Wireless Communication Systems."

Conference delegates are also encouraged to attend the opening and closing sessions of EuMC (which are also the main plenary sessions of the whole EuMW) on Tuesday and Thursday where

prominent speakers have been invited. Enrique Blanco, Global CTIO of Telefónica, Spain, will give a plenary talk on Tuesday, 25 September on 5G networks and communication systems. Giuliano Gatti, Galileo Space Segment Manager at European Space Agency (ESA), will contribute with a presentation about the Galileo global satellite navigation system during the closing session to be held on Thursday, 27 September. EuMC 2018 will close with the traditional awards ceremony, when the best paper prizes will be announced. Hopefully after the Week, you experience a higher motivation and passion for microwaves.

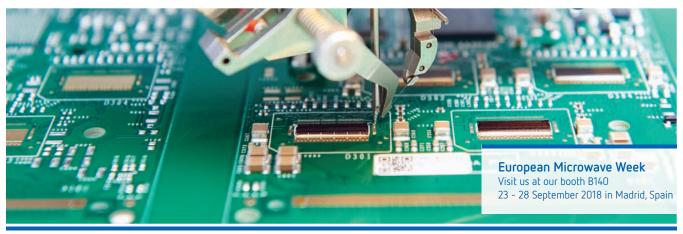


European Microwave Integrated Circuits Conference (EuMIC) 24-25 September

This is the 13th European Microwave Integrated Circuits Conference, EuMIC 2018. EuMIC arrives to Spain after a long journey that started in Rome in 1990, organized by the GAAS® Association, and continued, after 2004, in the framework of the EuMW.

The scientific conference is composed of 12 regular EuMIC sessions and three EuMC/EuMIC joint sessions covering topics from device to system level. mmWave technologies have gained an important presence in this edition, reflecting their role in paving the way for 5G and beyond. Device modeling is also present with four regular sessions, showing how a classic topic remains a challenge for our community. The five sessions on amplifiers will focus on system level issues. The interactive poster session has been organized jointly with the EuMC and will be held on Tuesday, enjoying the lively atmosphere of the exhibition. There are also short courses and workshops.

EuMIC has included three relevant industrial keynotes thanks to the kind participation of prominent speakers from Cree, GLOBAL-FOUNDRIES and Televés. Invited





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manufacturers will take the floor during the traditional "Foundry Session," hosted by the GAAS® Association. The EuMIC opening and closing plenary sessions will feature three invited speakers, world-class in their fields. During the opening ceremony Charles F. Campbell, engineering senior fellow with the Infrastructure and Defense Products Division of Qorvo, U.S., will present a realistic perspective of the present challenges that GaN monolithic designs faces. In addition, J. Sebastián Gómez Díaz, assistant professor in the Electrical and Computer Engineering Department of the University of California, Davis, U.S., will address the use of graphene and other 2D materials as a powerful, reconfigurable, CMOS compatible and miniaturized on-chip platform for THz device fabrication.

During the closing session William R. Deal, distinguished engineer in Northrop Grumman's RF and Mixed Signal Department, U.S., will talk about the status of transistor-based electronics operating above 100 GHz and will describe recent progress in communications and sensors at these frequencies. Also during the closing ceremony, the best contributed paper to EuMIC 2018 and the Young Engineer Prize will be awarded by the EuMIC Tech-

nical Program Committee and the EuMW Steering Committee. Three GAAS® Association PhD student fellowships will also be celebrated.

European Radar Conference (EuRAD) 26-28 September

This is the 15th edition of the European Radar Conference, after walking a path of continuous growth, both in absolute terms and its weight and significance within the EuMW. Top professionals will present their latest research and development, and discuss the present status and future trends in the fields of radar technology, system design and performance, radar components, radar propagation and target modeling, advanced sig-



nal processing techniques, as well as the most innovative radar architectures, concepts and applications. In the opening session on Wednesday, M. Carmen Barbero, from Indra Sistemas, will present their radar global concept for the next generation of F110 frigates for the Spanish Navy, in which advanced concepts such as full digital implementation using software-defined radio concepts and multiple function front-end sharing are included. Next, Dr. Stefano Pirandola, from the University of York, will present a more long-term vision of their technologies, exploring the capabilities of the quantum radar concept. For the closing session, keynote speakers, Domingo Castro, Rafael Casado and Jacobo Martínez-Villa, from Indra Sistemas, Spain, will describe the new radar facility for space debris surveillance that is starting to be installed in Spain.

This year, 156 papers were submitted to the conference, and after a rigorous selection process, the 93 accepted papers were organized into 22 oral sessions and two interactive sessions, some of them shared with EuMC. Prominent industrial keynotes speakers will open four of these sessions, showing the latest industry approaches to the addressed technologies. A special















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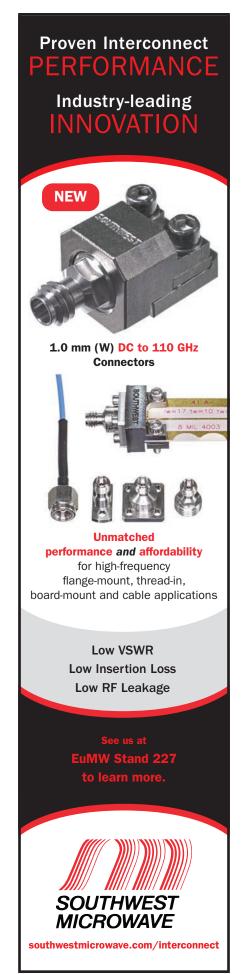
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session about radar projects in the European Defence Agency (EDA) has been organized by Dr. Roland Krebs, project officer, RF Sensor Technologies at EDA, to present their framework of R&T collaboration. The most relevant outcomes of recent projects in the frame of the RF Sensor Technologies CapTech will be presented by top level speakers, representing the European cooperation in this domain. An attractive topical workshops program will be running alongside the conference program.

Defence, Security and Space (DSS) Forum 26 September

The Defence, Security and Space Forum is jointly organized by the European Microwave Association (EuMA) and Microwave Journal, to complement EuMW's activity in the defence, security and space sector. This year, local input has been welcomed from: Fundación Círculo (Circle of Technologies for Defence and Security Foundation), TEDAE (Spanish Association of Technological Defence, Aeronautics and Space Companies) and UPM (Universidad Politécnica de Madrid). Each year the DSS Forum focuses on a hot topic that is engaging industry, academia and organizations/ agencies to develop, test and implement leading edge technology. This year's topic is "Integrating Unmanned Aerial Vehicles (UAV) into Defence and Security Scenarios." The popularity of UAVs is growing due to a reduction in costs and the increasing capabilities and benefits provided by such systems.

Currently, the estimated number of existing UAVs is believed to be a few million, with that figure estimated to grow exponentially in coming years. From a defense and security perspective, there is the need to provide UAVs with innovative technologies enhancing performances for safe and secure systems, and to defend against threats posed by terrorists and insurgents utilizing UAVs to achieve their own objectives. Microwave technologies are essential to meeting these challenges, by providing UAVs with

new and more advanced sensors and communications equipment. However, going forward, the development of such systems also anticipates the use of new technologies, such as big data and artificial intelligence, which will result in a high level of autonomy that using the data obtained by the sensors will provide the ability to learn from the environment and their own errors, eventually facilitating autonomous decision making in a constantly evolving environment.

Keynote speakers will consider the state of the art of leading technologies and systems for unmanned operations, the estimated evolution of technologies and trends and consider expected capabilities and functionalities to address future conflicts. The efforts made by the main players in the sector will be analyzed and their views on new trends and technological developments will be offered.

The industry session will reflect the effort and investment that is being made to innovate, develop and bring UAV technologies to market. Specific areas of activity include radar systems being developed for UAV security—detection, identification and denial and obstacle detection for autonomous flying and crash avoidance. From an industry perspective, the emphasis will be on development at system and sub-system level, with particular focus on sub-system integration, not forgetting the significant role that test and measurement has to play in moving the sector forward.







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At the end of the day, the Executive Forum will present the points of view of the different established and regulatory bodies that allow coexistence between the different aerial platforms and describe the activity of the different players already established and emerging in the field.

REGISTRATION

Delegates can register for one, two or all three of the conferences. Registration at one conference does not allow any access to other conference sessions. Those who wish to register for two or more conferences will receive a discount on these registrations.

INTERACTIVE SESSIONS

The interactive poster papers will be presented on electronic screens, which are located in the conference area on Monday and Friday, and in the exhibition as signposted on Tuesday, Wednesday and Thursday.

EXHIBITION

The exhibition area will be located in Hall 9 (North Entrance) and comprised of more than 250 companies and organizations showing off their latest technologies and products. The exhibition area will also host the MicroApps Sessions and Exhibitor Workshops. The MicroApps will be three days of sessions given by various experts from exhibiting companies. The Exhibitor Workshops will be made up of instructional presentations, such as amplifier and filter design, in addition to the basics of making RF and mmWave measurements. As a registered delegate you will have full access to the exhibition area so be sure to take time and see what new products and technologies the industry is offering.

Exhibition Hours

Tuesday, 25 September 9:30–18:00 (followed by the Welcome Reception) Wednesday, 26 September 9:30–17:30 Thursday, 27 September 9:30–16:30

EVENTS

EuMIC Get-Together

<u>Date:</u> Monday, 24 September <u>Duration:</u> 20:00–22:00 <u>Location:</u> Larumbe, La Terraza, 4th Floor, Centro Comercial ABC Serrano, Serrano 61 <u>Cost:</u> Free to EuMIC delegates

Following the tradition of the EuMIC, delegates are invited to enjoy an informal dinner that will be offered by a first-class catering service in a unique location—Edificio ABC Serrano. A 19th century building located in the heart of Madrid, facing Serrano Street and Paseo de la Castellana, Edificio ABC Serrano is an unrivalled setting to have a good time with colleagues and friends, and taste the excellent Spanish cuisine.

Welcome Reception

<u>Date:</u> Tuesday, 25 September <u>Duration:</u> 18:30–21:30 <u>Location:</u> Palacio del Negralejo, Ctra. San Fernando a Mejorada, km 3, 28522 Rivas-Vaciamadrid <u>Cost:</u> Free to conference delegates & invited exhibitors

All registered conference delegates, as well as invited representatives from companies participating in the exhibition, are invited to the EuMW 2018 Welcome Reception, sponsored by Keysight Technologies, Horizon House Publications and EuMA. Delegates will need to bring their badge and exhibitors their invite along with them to gain entrance. The evening will begin with drinks at 18:30 followed by the General Chairs' handover from EuMW 2018, Madrid to EuMW 2019, Paris as well as an address from the Platinum Sponsor, Keysight Technologies. The open-buffet dinner will be served at 19:00. Bus transportation to and from Palacio del Negralejo will be provided.

Private Visit to the Thyssen-Bornemisza Museum and Cocktail Dinner

<u>Date:</u> Wednesday, 26 September <u>Duration:</u> 19:30–21:00

<u>Location:</u> 17.30–21.00 <u>Location:</u> Museo Thyssen-Bornemisza,

Paseo del Prado, 8

<u>Cost:</u> €45 for delegates, €60 for exhibitors



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A private visit to the Thyssen-Bornemisza Museum, one of Madrid's Golden Triangle of Art together with the Prado and the Reina Sofía national galleries, has been organized, followed by a cocktail dinner. With over 1,600 paintings and sculptures, the Thyssen-Bornemisza was once the second largest private collection in the world, after the British Royal Collection. The Museum now houses the core of the collection and fills the historical gaps in its counterparts' collections. Guides will be available through the different rooms of this magnificent museum. This unique experience will be complemented with a cocktail dinner. Subsidized tickets, €45 for delegates and €60 for exhibitors, are limited, so register as soon as possible.

Young Professionals Meet-Up

Date: Thursday, 27 September **Duration: 19:30-22:00**

Location: A downtown Cafeteria, TBA

Cost: Free to all YPs

EuRAD Lunch

Date: Friday, 28 September Duration: 12:30-13:50 Location: Retiro Toom, IFEMA Cost: Free to EuRAD delegates and Friday WS/SC delegates

HOTEL RESERVATIONS

Horizon House has teamed up with Connex Hotels and Events, the official hotel booking supplier, to offer you the

ability to reserve your accommodation for EuMW 2018 at the most competitive rates available. Visit connexhotelsandevents.com/eumw-2018-madrid. html or email sally@connexhotelsandevents.com to make your accommodations. You will find a wide range of offerings to suit every budget.

GETTING TO IFEMA-FERIA DE MADRID CONVENTION CENTRE

The city of Madrid is located in the geographic center of Spain and it is well connected to the European motorway, rail and flight networks. IFEMA-Feria de Madrid Convention Centre can be accessed through a variety of transportation means. Madrid-Barajas Airport is located only 10 minutes from the exhibition complex, and just 15 km from the city centre which it is connected by Metro (airport stations T-1, T-2, T-3 and T-4).

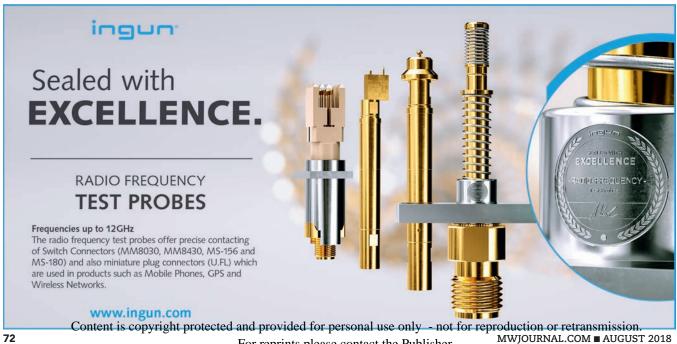
Access to Feria de Madrid is possible from anywhere in the city by means of Feria de Madrid station on Line 8, whose exit is at the South Entrance of the complex. Line 8 also connects the venue with the different terminals of Baraias International Airport. A wide bus network provides access to Feria de Madrid from different points in the city: Route 112-Feria de Madrid-B° Aeropuerto. Route 122-Avda. de América-Feria de Madrid. Route 828 Universidad Autónoma-Alcobendas-Canillejas-Feria de Madrid.

In order to facilitate the delegate transportation to and from IFEMA, a shuttle bus route has been organized from local hotels as well as from the South Entrance (metro) to the North (EuMW) Entrance. For the complete time tables, please check the EuMW website.

ENJOY MADRID

The first historical record of Madrid dates back to the year 865, when Emir Muhammad I commissioned the construction of a fortress in the village of Mayrit, on the banks of the river Manzanares. Mayrit means "plenty of waterways," and belonged to the Islamic world until 1083, when Alfonso VI of Castile took over the city.

Today, Madrid is a dynamic business center that goes hand-in-hand with its vibrant atmosphere, tourist appeal and passionate cultural and recreational life. While visiting, discover its historical sites, iconic museums and spectacular range of restaurants, plus enjoy its endless nightlife and the flood of designs, fashion and trends you will find in the shops of one of Europe's leading capitals. A great city that boasts a rich treasure of art, culture and natural environments, set in a region packed with history and modernity. Visit esmadrid.com/ en for information on top attractions and tips for your stay.■





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| Frequency, GHz Signal genera | tors | J0SSAG11 5.9 - 12.0 | J0SSAG12 10.0 - 18.0 | J0SSAG13 17.0 - 24.3 | J0SSAG14 24.0 - 40.0 | | DISCOUN |

Wednesday, 26 September – IFEMA Feria de Madrid, Spain

A one-day focused Forum addressing the integration of unmanned aerial vehicles (UAV) into defence and security scenarios.

The popularity of Unmanned Aerial Vehicles is growing due to a reduction in costs and the increasing capabilities and benefits provided by such systems. Currently, the estimated number of existing UAVs is believed to be a few million, with that figure estimated to grow exponentially in coming years. From a Defence and Security perspective, there is the need to provide UAVs with innovative technologies enhancing performances for safe and secure systems, and to defend against threats posed by terrorists and insurgents utilizing UAVs to achieve their own objectives.

Programme:

08:30 - 10:10 EuRAD Opening Session

10:10 - 10:50 Coffee Break

10:50 – 12:30 New Concepts, Technologies and Systems for UAV Integration and Their Role in Future Hybrid Scenarios

Moderator: Alfonso Farina, IEEE Fellow

- Technological Demonstrator of Enhanced Situation Awareness in Naval Environment with the Use of Unmanned Systems
- Dr. Tony Arecchi, Ocean 2020 Project Coordinator, Leonardo S.p.A.
- UAV Integration: European and Spanish Situation, Challenges and Potential Solutions
- Isabel Maestre, Executive Director of Spanish Aviation Safety and Security Agency (AESA)
- Anti-UAV Defence Systems Miguel Acitores, Director of Security Business Development, Indra

12:40 – 13:40 Strategy Analytics Lunch & Learn Session

The Implications of Expanding the UAS Mission Envelope in Military and Civilian Airspace – Asif Anwar, Strategy Analytics

13:50 – 15:30 Microwave Journal Industry Panel Session

This session offers a perspective on the endeavour, innovation and investment that industry is committing to the development of UAVs in the defence and security sector. Speakers will offer an insight into such areas of activity as microwave sensors/sub-systems, the test and measurement challenges that are being addressed and the issue of UAV identification and detection.

- Improving the SWAP-C Advantage in UAVs for Defense & Security Dean White, Qorvo
- Designing Systems and Sensors for Counter Drone Operations Tobias Willuhn, R&S
- Radar Systems for UAV Detection R. Cardinali, A. Di Lallo, A. Farina, G. Palumbo, L. Timmoneri, and D. Vigilante
 Leonardo, Land & Naval Defence Electronics/Security and Information Systems
- Detect and Avoid: An Industrial Perspective Technical and Certification Considerations for UAVs
- Andrea Maccapani and Maurizio Goiak, Leonardo S.p.A., Airborne and Space Systems Division

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Room N101-N102, 08:30 to 18:30







15:30 – 16:10 Coffee Break

16:10 – 17:50 Round Table: Efforts & Investment Needs to Drive UAV Technologies to Market

High level speakers from key governmental agencies and commercial companies involved in the development of UAV systems and technologies and their implementation and integration into security and defence markets will offer their opinions and outline the opportunities and challenges that can be expected in coming years. Speakers will also focus on the research needs and technological trends that will define the architectures and technical characteristics of future unmanned systems. Moderator: Ignacio Montiel, Project Officer Information Technologies, European Defence Agency (EDA). Speakers: Paolo Salieri, Principal Scientific and Policy Officer in the Directorate General for Enterprise and Industry of the European Commission. Fernando Mijares, Head of Future Projects of AIRBUS Defence & Space. Juan Besada, Professor, Information Processing and Telecom Center, Universidad Politécnica de Madrid (IPTC-UPM). Member of SESAR Scientific Committee. Fernando Arias, Senior Expert, ISDEFE.

17:50 – 18:30 **Cocktail Reception**

Registration fee is \in 20 for those who registered for a conference and \in 60 for those not registered for a conference.

The Conference Special Events section of the EuMW website will give further details and updates.

Organized by:





The Spanish Microwave Industry: Specialists in Space, Defense & Telecoms

Helen Duncan MWE Media Ltd., U.K.

> or many of us in the wireless and microwave community, the mention of Spain initially brings to mind Mobile World Congress (MWC), the huge trade show in Barcelona that attracts around 100,000 visitors each February. However, Spain has had a thriving RF and microwave industry of its own since well before MWC relocated there over a decade ago, and it is currently growing rapidly. The country's particular strengths include aerospace, defense and antennas, as well as telecoms, and this article will highlight just a few of Spain's companies and institutions, along with the developments they are contributing to the European microwave community.

> It has been 25 years since the European Microwave Conference (EuMC)—then a much smaller event than the present, multi-

conference European Microwave Week (EuMW)—last took place in Madrid in 1993, and as the conference returns there, we reflect on some of the changes Spain's market has seen in the intervening years. *Figure 1* shows the Puerta de Alcalá in Madrid, one of dozens of stunning historical monuments and buildings in Spain's capital city that people can visit while attending the conference.



Fig. 1 European Microwave Week 2018 will take place in Madrid, Spain, on 23–28 September.

EARLY 5G DEPLOYMENTS

Possibly the company name most familiar to the wireless industry is **Telefónica**, the Spanish-headquartered, multinational telecoms operator that is parent to the O2 and Movistar brands in Europe and Latin America. In addition to its mobile networks, Telefónica has operations in satellite media distribution in Spain and Latin America, and also a chain of R&D centers located around the world.

Telefónica announced in January this year that it is progressing well along the path to 5G with early deployments in two Spanish cities—Segovia and Talavera de la Reina—in partnership with Nokia and Ericsson. Under the 5G Technological Cities project, these two cities will become "living laboratories" for developing the capabilities of 5G. The plan is to deploy the network over the next three years, increasing peak data speeds over mobile to 10 Gbps and reducing latency to less than 5 ms, while in parallel carrying out testing of new use cases. Initially the network will be non-standalone 5G NR, supported by the existing 4G network, but will eventually evolve to a standalone 5G

An open research and innovation laboratory called **5TONIC**, located in Madrid, is a joint venture between Telefónica and Imdea Networks that aims to create an open environment where industrial and academic par-

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ticipants from around the world can work together on research projects related to 5G technologies.

Telefónica I+D, the research and development company of the Telefónica Group, also has a technology center in Madrid, as well as offices in Barcelona, Granada, Huesca and Valladolid in Spain and in other locations around the world. Its mis-

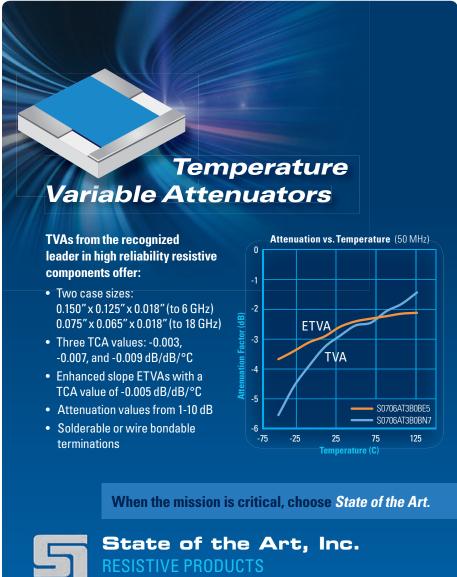
sion is to help improve the Group's competitiveness and to keep up-todate with technological innovation, as well as developing new products and services. Not surprisingly, its current projects include 5G and M2M developments, longer-term innovation programs on human behavior and mobility and on future networks as well.

Telefónica's Global CTIO, Enrique Blanco, will present a keynote address in the EuMW 2018 Opening Session, outlining how 5G technologies will impact future communication networks.

SPACE AND DEFENSE

Spain has long been an influential player in the defense and aerospace sector, with many Spanish companies being active contributors to various European Space Agency (ESA) programs. Madrid is home to three divisions of the aerospace giant Airbus, including Airbus Defense and Space (Airbus DS) that incorporates Airbus DS-CASA Espacio—formerly part of EADS-Astrium. This company specializes in antenna design for satellites, radiometers and radar.

Carlos Montesano, senior expert on antennas and head of R&D at Airbus DS, said, "Our satellite antenna developments are focused in two main areas, large reflector parabolic antennas and active arrays." Montesano identified important trends in this field towards larger antennas with greater numbers of beams, which give more flexibility in arranging channel contracts with terrestrial operators. In active arrays, one of the company's most important projects is the receive antenna for the Eutelsat Quantum¹ satellite, billed as the first fully flexible telecom satellite. Eutelsat Quantum offers both Ku-Band channels for commercial use and X-Band channels for government applications. The active array architecture means that coverage, bandwidth, power, frequency and orbital slot are all reconfigurable in orbit, allowing Quantum to serve any region of the world and





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Fig. 2 The MWR K/Ka-Band radiometer developed by Airbus DS-CASA measures atmospheric propagation delay over the ocean.



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|---|---|-------------------|---------------|---------------|----------------|---------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|--------------------|--|
| í | Dynamic Range (BW=10Hz, dB, typ) (BW=10Hz, dB, min) | 120 110 | 120 110 | 120 110 | 120 110 | 120 110 | 120 110 | 120 110 | 115 100 | 115 105 | 100 80 | 110 100 | 100 80 | 65 45 | |
| | Magnitude Stability (±dB) | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.25 | 0.25 | 0.3 | 0.3 | 0.5 | 0.5 | 0.8 | 0.5 | |
| | Phase Stability (±deg) | 2 | 2 | 2 | 2 | 2 | 4 | 4 | 6 | 6 | 8 | 8 | 10 | 6 | |
| 4 | Test Port Power (dBm) | 10 | 13/6 | 13/6 | 11/6 | 6 | 9 | -1 | -2 | -6 | -10 | -8 | -25 | -30 | |



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RADIOMETERS AND RADAR

Airbus DS's current radiometer programs in Madrid include the MWR nadir-looking sounder and the ICI mmWave instrument, which

is being developed for the remote sensing of high altitude ice clouds. MWR, shown in Figure 2, operates at 23.8 and 36.5 GHz (K/Ka-Band), covering a bandwidth of 200 MHz in each channel and is designed to measure water vapor and cloud water contents in the field of view of the altimeter, in order to com-

pensate for the propagation delay these cause in radar measurements. It does this by measuring the brightness temperature of the Earth's radiation. These corrections can only be made over the ocean, where the background noise is stable and can be measured. Over ice and land surfaces, wet troposphere corrections based on global meteorological data and dedicated models are used instead.

Airbus DS-CASA Espacio was selected by ESA as the prime contractor for the ICI instrument, which is a total power sub- and mmWave conically scanning radiometer. It provides brightness temperature measurements in 11 heterodyne receiver channels, including two dualpolarization channels, ranging from 183 to 664 GHz. It is designed to monitor the exchange mechanisms in the Earth's upper troposphere and lower stratosphere, focusing in particular on the remote sensing of high altitude ice clouds. Although this technique for measuring ice clouds was first proposed in 1995, this will be the first radiometer of its kind to have been developed for Earth observation from space.

Another recent Airbus project, PAZ—the radar satellite of the Spanish National Earth-Observation Program—was launched earlier this year by a SpaceX Falcon 9 rocket. The PAZ satellite, shown in Figure **3**, was primarily intended to address civilian surveillance needs as well as to cover defense and security applications. "Paz" is the Spanish word for peace.

Using Synthetic Aperture Radar (SAR) imaging instead of a camera, the satellite is able to capture images with equal clarity by day and



Fig. 3 The PAZ satellite uses SAR to collect images day and night for both military and civilian applications.

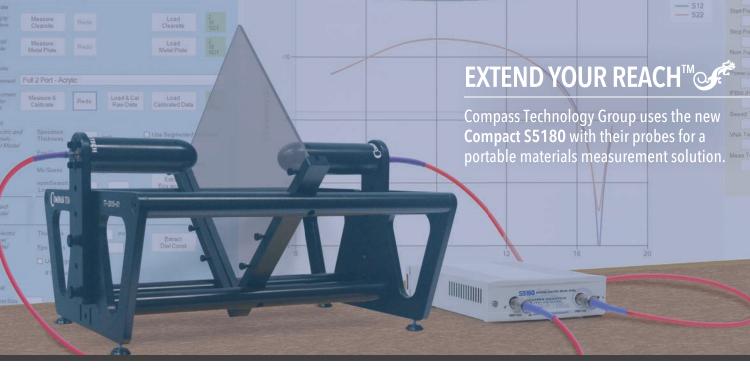


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S5180 Compact VNA Specifications:

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▶ Two-Port Two-Path

Dynamic Range: 120 dB min, 130 dB typ. (10 Hz IF)

▶ Measurement Time Per Point: 30 µs typ.

▶ Measurement Points: 2 to 200,001

The **Compact Series** includes instruments for a wide array of applications with frequencies from 9 kHz to 18 GHz* allowing engineers to extend their reach.

Compact USB VNA models available in 50 or 75 Ohm *Frequency depends on model

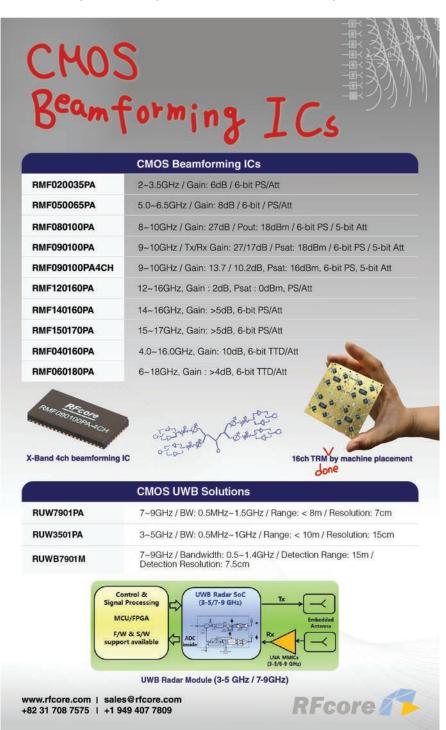
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night under any meteorological conditions. Operating in the military X-Band spectrum, it can capture more than 100 images each day with up to 1 m resolution. During its five-and-ahalf year mission, PAZ will cover an area of over 300,000 km² per day from its slightly inclined quasi-polar orbit, covering the entire globe on

average in 24 hours. Its diverse range of tasks include: terrestrial monitoring; high resolution cartography; border control; tactical international support; crisis management; risk analysis; evaluation of natural disasters; environmental control; marine environment analysis; and marine wildlife monitoring.



PARTICLE ACCELERATOR COMPONENTS

Tryo Group is a Spanish-headquartered RF and microwave specialist, consisting of two divisions-Tryo Aerospace and RYMSA RF and has facilities in Madrid as well as in other cities including Bilbao and Barcelona, along with international offices. Figure 4 shows an anechoic chamber, part of Tryo Group's facilities for the design and qualification of antennas and RF equipment for both broadcast and space applications. Tryo Aerospace designs and manufactures antennas and subsystems, while the product portfolio of RYMSA RF includes antennas, filters, combiners and air traffic control systems.

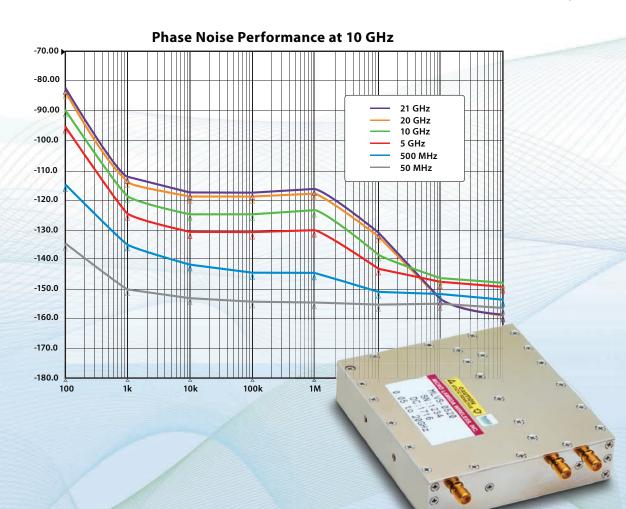
In recent months, RYMSA has secured contracts with two important European scientific organizations for components for particle accelerators. In May, the European Organization for Nuclear Research (CERN) selected RYMSA as its sole supplier for the manufacturing, integration and cabling of 2,752 sets of output filters and high frequency transformers for the proposed upgrading of the modular converter R2E-LHC, which is a key component of the Large Hadron Collider.

In a similar application, the GSI Helmholtz Center for Heavy Ion Research (GSI) in Germany selected RYMSA for the supply of several 9 3/16 EIA directional couplers and coaxial parts for the RF powerlines of GSI/FAIR Proton LINAC (linear accelerator) project. The seven RF powerlines each feed the RFQ cavity with 2.5 MW of forward power and a maximum of 5.5 MW of reflected power at a frequency of 352 MHz.



Fig. 4 Tryo Group has facilities for the design and qualification of antennas and RF equipment for both broadcast and space applications.

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US patents #9,793,904 B1, #9,734,099 B1

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For more information contact Micro Lambda Wireless.

www.microlambdawireless.com

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In June of this year it was announced that Tryo Group had been acquired by Sener, a Spanish engineering and construction group with a division specializing in aerospace. The merger brings together aerospace businesses with a combined turnover of almost €120 million.

AIRBORNE AND UNDERWATER

Indra Sistemas is a Spanish multinational IT and defense systems company headquartered in Madrid. With a broad portfolio in developing end-to-end technology in fields such as defense and security, transportation, energy, telecommunica-

tions and media and healthcare, the company has a total turnover of more than €3,000 million.

Indra is particularly active in airtraffic control systems and radar and the company will exhibit at EuMW 2018. Miguel Acitores, Indra's director of security business development, will speak in the Defence, Security & Space Forum on Wednesday, 26 September on the topic of anti-UAV defense systems. Indra speakers will be featured in both the opening and closing sessions of EuRAD: Maria Carmen Barbero, head of naval radar programs, will present the new radar generation for the F-110 frigate integrated masts, focusing specifically on the advances made in the development of the primary S- and X-Band radar, secondary radar and other sensors. Jacobo Martínez-Villa will describe the S3T Spanish ESA radar facility for space debris surveillance that is just starting to be installed. There will also be a speaker from Indra in the EuMW Career Platform session on Tuesday, 25 September.

TTI has its headquarters in Santander on the North coast of Spain, supported by additional facilities in Madrid and Seville. It specializes in designing and developing customized antennas ranging in frequency from L- up to Ka-Band. These include printed antennas for linear and circular polarizations, active phase array antennas and waveguide and horn antennas, many of which are aimed at SATCOM applications. Complete hybrid systems in X-, Ku- and Ka-Bands are also produced for "on-the-move" SAT-COMs.

TTI is a member of the EU SWARMs consortium, for the robotic remote control and operation of unmanned underwater and surface vehicles. Final integration and validation were performed for the European Commission at Trondheim in Norway during June of this year. These final tests demonstrated the performance of integrated acoustic and radio communications networks for two autonomous underwater vehicles (AUV) and a unmanned surface vehicle (USV), including both





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RF Power Amplifier Design Techniques October 24-26, San Jose, CA - Ali Darwish

5G Wireless Networks

October 22 - 24, San Jose, CA - Joe Boccuzzi

Transceiver and Systems Design for Digital Communications Feb 25-Feb 27, 2019, San Diego, CA - Scott Bullock

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Ultra-Low Phase Noise OCXOs 10 and 100 MHz

MV317 100 MHz, +5V/+12V

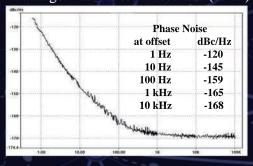
- Temperature Stability: 1E-8
- Aging: ±1E-7 per year
- Package: 25.8x25.8x10.3 mm



| dBr | | MV317 | |
|-------|----------|-----------|--------|
| 110.0 | | Phase | Noise |
| | | at offset | dBc/Hz |
| 20.0 | <u> </u> | 10 Hz | -107 |
| 130.0 | | 100 Hz | -137 |
| 140.0 | | 1 kHz | -165 |
| 50.0 | | 10 kHz | -176 |
| 160 0 | | 100 kHz | -180 |
| 170.0 | | | |
| 180.0 | | | |
| 190.0 | 100.00 | | |

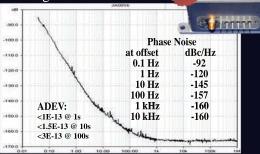
MV272M 10 MHz

- Temperature Stability: 1E-9
- Allan Deviation: <4E-13 per sec.
- Package: 41.0 x 30.0 x 17.0 mm (SMD)



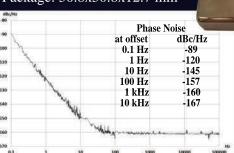
MV336 10 MHz, +12V

- Temperature Stability: 2E-11
- Aging: ±1E-8 per year
- Package: 92x80x50 mm



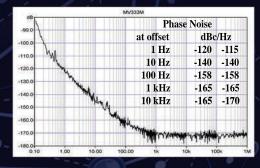
MV341 10 MHz

- Temperature Stability: 1E-9
- Allan Deviation: <2E-13 per sec.
- Package: 50.8x50.8x12.7 mm



MV333M 10 MHz

- Temperature Stability: 3E-9
- Allan Deviation: <5E-13 per sec.
- Package: 25.8x25.8x12.7 or 36x27x16 mm



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remote control of the USV and the execution of specific AUV missions controlled from the onshore command and control center.

AMPLIFIERS

ERZIA, which has its headquarters in Santander, makes microwave and mmWave modular high-power and low-noise amplifiers, and also integrated subsystems, operating up to over 100 GHz. Its portfolio includes a range of standard amplifier modules, as well as offering customization for both amplifiers and high-specification integrated assemblies for aerospace, commercial, military and scientific systems.

Applications have included electronic warfare (EW) systems for a number of European defense system main integrators for land, air and naval platforms, and space-qualified amplifiers and systems have been supplied for missions such as LISA Pathfinder, Change 3 and 4, SEOSAR PAZ, Exomars and Venus Express. Another product line is long-range line-of-sight datalink systems for unmanned aerial vehicles (UAV) and combat aircraft, which has been flight qualified on F-16 fighters.

ERZIA will introduce at EuMW 2018 its latest product line of X-Band pulsed solid-state power amplifiers (SSPA) for radar applications. Based on GaN devices, the new SSPAs have output powers of 50, 100, 200 (see *Figure 5*) and 400 W, and are part of a range that already included CW SSPAs and space-qualified amplifiers at X-Band. The company will also give a presentation at the MicroApps seminar about its high-power X-Band amplifier design work.



♠ Fig. 5 200 W X-Band pulsed SSPA for radar applications, being launched by ERZIA at EuMW 2018.

ANTENNAS

Barcelona-based Fractus Antennas SL designs, manufactures and commercializes miniature, off-theshelf antennas for smartphones, short-range wireless and connected IoT devices. Founded as an independent antenna product business in 2015, Fractus Antennas was born out of the main Fractus operation, and combines a respected R&D team with proven manufacturing capabilities and scale to bring to market a new generation of antenna products to meet the mobile and wireless connectivity needs of OEMs. Fractus Antennas' most recent launch was a new reference design that explains how to use the TRIO mXTEND™ chip antenna component to get the GNSS and Mobile frequency bands at the same time. TRIO mXTEND™ is the newest member of the Virtual Antenna™ family and it is also the only one with a multiport configuration.

RESEARCH CENTERS

The industrial and manufacturing base in Spain is supported by an active research base, both in universities and research institutions, many of which are involved in a number of EU-sponsored R&D programs.

The Universidad Politécnica de Madrid (UPM, Polytechnic University of Madrid) is the highest-ranked technical university in Spain, and, as well as its degree programs, it is very active in a number of EU projects in telecoms and microwave technology. Naturally, as the event is taking place this year in its home city, UPM has a number of representatives on the EuMW 2018 Organizing Committee.

Ceit-IK4 is a non-profit research center that was set up in 1982 by the University of Navarra with a mission to work closely with the R&D departments of industrial clients to carry out applied research projects. It also has an academic role in training doctoral students within the framework of industrial research projects, and in publishing and disseminating non-confidential results. One of its projects is the IoTSpace initiative, an open laboratory to



promote training and innovation in young researchers working on reallife projects related to the IoT.

25 YEARS ON

For an overview of the microwave industry in Spain, and how it has changed over the past 25 years, I spoke with Michael Chadwick of **SpanTech**, a specialist distributor of microwave components that was first launched onto the market at the 23rd EuMC in Madrid in 1993, and will celebrate its 25th anniversary by exhibiting at this year's event.

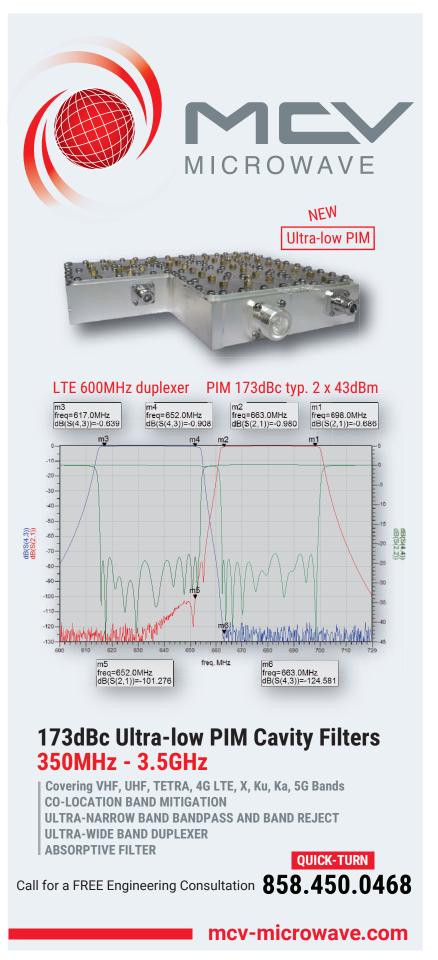
"The RF and microwave industry in Spain has changed beyond all recognition since 1993, when there was a limited market here, mostly for standard components. Now Spain is challenging the market in integrated systems as well as exporting leading-edge microwave components," said Chadwick.

In conclusion, the RF, microwave and mmWave market in Spain seems particularly buoyant at the moment, fueled by a growing level of European and global investment in satellite technology, which is one of Spain's traditional areas of excellence. In contrast to the 1993 exhibition, which was a small and somewhat niche event, the breadth of technology expected to be on show at EuMW 2018 reflects how much this core microwave expertise has spun out into telecoms and wireless. This has positioned Spain among the leaders in developing 5G technology, as well as retaining its status in aerospace and defense applications.

| 1.1 | |
|--------------|--------------|
| Company | EuMW Stand # |
| 5TONIC | Stand 284 |
| Indra | Stand 16 |
| TTI | Stand 248 |
| Airbus DS- | |
| CASA Espacio | Stand 141 |
| ERZIA | Stand 12 |
| Tryo | Stand 214 |
| Spantech | Stand 335 |

Reference

 Eutelsat Quantum, http://news.eutelsat.com/blog_posts/four-things-youshould-know-about-eutelsat-quantum 40079



For complete coverage of the EuMW 2018 conference, event news, exhibitor product information and special reports from the editors of *Microwave Journal*, visit our online show daily at mwjournal.com/eumw2018.

CST

Stand 21

VENDOR**VIEW**CST STUDIO SUITE



CST STUDIO SUITE is a package of high performance software for the simulation of EM fields in all frequency bands. Its growing success is based on a combina-

tion of leading edge technology, user-friendly interface and knowledgeable support staff. CST solutions are used by market leaders in a diverse range of industries including aerospace, automotive, defense, electronics, healthcare and telecommunications. CST is part of SIMULIA, a Dassault Systèmes brand.

www.cst.com

Rohde & Schwarz GmbH & Co. KG

Stands 23. 26

VENDORVIEW Automotive Radome Tester



Integrating automotive radar sensors into cars is very challenging. Radars operate behind bumpers, design emblems or other plastic parts. All radome materials

need to be sufficiently transparent and homogeneous for automotive radars. Rohde & Schwarz has developed the R&S QAR quality automotive radome tester, a tailored solution for radar integration testing. It is a mmWave imaging system operating in the E-Band automotive frequency range. Thanks to its spatially resolved reflection measurement capability, it provides a very intuitive yet powerful way to evaluate radome performance.

www.rohde-schwarz.com

Maury Microwave

Stand 28

Measurement and Modeling Device Characterization Solutions



Exceptional companies have superior labs—complete your lab with Maury Microwave! Maury, a leader in measurement and modeling device characterization solutions, VNA calibration accessories and interconnections, will be showcasing active

and hybrid-active harmonic load pull solutions, LXI™-certified mechanical impedance tuners, pulsed IV/RF compact transistor modeling as well as coaxial and waveguide VNA calibration kits and metrology adapters, in-stock color-coded precision and daily-use adapters and test-port, phase-stable and value cable assemblies. Visit the company for details, demos, deals and NPIs!

www.maurymw.com

Copper Mountain Technologies Stand 35

S5180 VNA



The S5180 VNA delivers lab grade performance in a compact package. This portable network analyzer can be battery powered and used in the field, in the laboratory, and in production testing. S5180 VNA includes an RF measurement module and software application which runs on a PC, laptop or tablet, connecting to the measurement hardware via USB interface. Software can be installed on multiple computers, making it easy to share the use of the analyzer measurement module.

www.coppermountaintech.com

NI AWR

Stand 101

VENDOR**VIEW**Design Environment V14



Visit Stand 101 to preview NI AWR Design Environment V14, featuring network synthesis for developing impedance matching circuits of multi-band amplifiers and more, enhanced

automation for editing imported PCB designs, new capabilities for EM analysis and an expanded phased-array/MIMO antenna wizard. The NI AWR Design Environment platform includes Visual System Simulator™ system design software, Microwave Office/Analog Office circuit design software and AXIEM and Analyst™ EM simulators. The broader NI AWR software portfolio also includes AntSyn™ antenna synthesis software and AWR Connected™ third-party solutions.

www.ni.com/awr

Stand numbers are complete at the time of going to press.

HUBER+SUHNER

Stand 130

VENDOR**VIEW**Multicoax Testing Solutions



HUBER+SUHNER offers a broad range of high-end RF test components and assemblies, developed and optimised for high

speed digital testing. Its latest MXPM multicoax testing solution is a pioneering and future-proof solution that supports testing up to 67 GHz (with option to 85 GHz). By offering a high density (2.5 mm) pitch, the MXPM guarantees a satisfying experience with its user-friendly magnet mount connection, making performance and reliability affordable. It allows eight or 16 channel measurements.

www.hubersuhner.com

Ingun

Stand 130

RF Test Solution for IoT & 5G



The HFS-856 series offers a reliable RF test solution for IoT and 5G applications. Unlike OTA measurements, the signal can

be tapped directly from the PC board. The mechanical sturdiness makes it suitable for harsh production environments. The test probes have particularly good, repeatably-accurate RF features. The VSWR is at least 1.3 in specified frequency ranges, the insertion loss is maximum 0.6 dB. A SMA connector or, for smaller grid sizes, a SMPM (-T) connector is used to connect the probes to the test system. A flange makes assembly in test fixtures especially easy. Tolerances are balanced out of by the test probe's floating mount. The modular design allows the test probes to be modified for other applications.

www.ingun.com

WIN Semiconductors USA

Stand 137

0.45 µm GaN Power Process for 5G Applications



WIN Semiconductors has expanded its GaN process capabilities to include a 0.45 µm-gate technology that supports current and future 5G

applications. The NP45-11 GaN on SiC process provides 50 V operation with superior power density and efficiency. It allows customers to design hybrid Doherty

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power amplifiers used in 5G applications including massive MIMO wireless antenna systems. Similar to macro-cell applications, MIMO base stations often combine Doherty power amplifiers with linearization techniques to meet demanding linearity and efficiency specifications of today's wireless infrastructure.

www.winfoundry.com

RFMW

Stand 139

VFNDORVIEW RF Energy Pallet Amplifier



Ampleon's BPC-2425M9X2507 Power Module offers 250 W CW power for RF cooking applications at 2450 MHz. With 61%

efficiency and 17 dB gain, this high efficiency module has integrated temperature sensing and bias temperature compensation networks. Operating from a 32 V supply, the input and output are matched to 50 ohms for ease-of-use, providing a cost effective solution with minimum design work and easy connectivity in multi-pallet applications.

www.rfmw.com

Cicor Group

Stand 140

DenciTec®



DenciTec®enables the production of very high-density circuits. DenciTec®makes further miniaturization possible. Possibilities

include line widths and spacings down to 25 μm (1 mil) with copper thicknesses of 20 μ m (0.8 mil) \pm 5 μ m on all conductive layers, laser-via diameters of 30 µm (1.2 mil), annular rings of 30 µm (1.2 mil) for the inner layers and 20 µm (0.8 mil) for the outer layers. Cicor complements its spectrum of services with a solution that delivers highly miniaturized circuits of the highest reliability.

www.cicor.com

Southwest Microwave

Stand 227

1.85 mm PCB Compression Mount Connector

This new 1.85 mm (67 GHz) PCB compression mount connector requires no solder, is designed for microstrip or grounded coplanar designs and provides the superior performance only a Southwest Microwave



connector can offer. This connector can be vertically attached anywhere on the PCB surface and has no PCB thickness limitations. As with all Southwest Microwave PCB mount connectors, board layout

assistance is available upon request. www.southwestmicrowave.com

Focus Microwave Group

Stand 231

2 kV Pulsed IV Characterization



Design and test engineers are looking for high performance, robust, narrow pulsed IV solutions. Auriga's new PHD2000-100 drain pulser head. available with the

newly redesigned AU-5 Pulsed I-V measurement system, allows for pulsed DC characterization up to 2000 V and 100 A. This new high voltage offering is designed to meet the ever-changing requirements and is poised to handle the increasing demand from various industry verticals which include automotive, medical, industrial and telecommunications.

www.focus-microwaves.com

Coilcraft

Stand 253

Ceramic Wirewound Chip Inductors



Coilcraft's new 0402DC Series ceramic wirewound chip inductors offer the industry's highest Q factors in an 0402

(1005) size—up to 162 at 2.4 GHz—for super low loss in high frequency circuits. They are offered in 26 standard inductance values ranging from 3 to 120 nH. An additional 73 values are available upon request, including 0.1 nH increments from 2.8 to 10 nH. Most values are available with 2 percent tolerance.

www.coilcraft.com/0402dc.cfm

SPINNER GmbH

Stand 266

VENDORVIEW Low PIM Switching Matrix

With the new SPINNER Low PIM Switching Matrix you can speed up testing in production, for

example of mobile communications antennas or filters. It lets you easily boost your output by concurrently measuring PIM and VSWR on separate test paths. And that is not all: thanks to the exceptional reliability of every measurement, you avoid having to frequently repeat tests to compensate for uncertain results. Visit SPINNER at Stand 266.

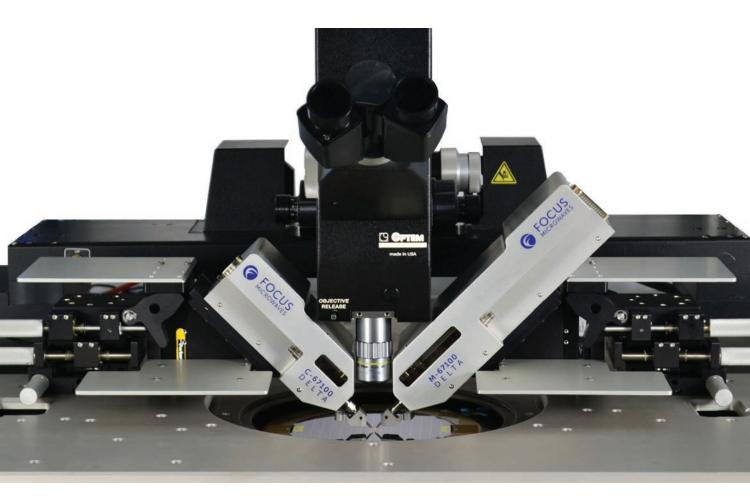
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Rosenberger

Stand 270

Test & Measurement



At EuMW 2018, Rosenberger highlights its latest test & measurement developments-equipment and devices for microwave and VNA

measurements, calibration kits (full and industrial version), compact calibration kits such as MSO (open, short, load) and MSOT (open, short, load, thru), microwave cable assemblies and VNA test port cable assemblies, multiport mini-coax and spring loaded coax products for semiconductor testing or PCB connector systems. For aerospace applications the company provides coaxial connectors qualified according ESCC and DIN EN 9100.

www.rosenberger.com

Spectrum Elektrotechnik GmbH Stand 281

Hermetically Sealed Adapters

Spectrum Elektrotechnik GmbH offers a wide range of hermetically sealed adapters to the hermeticity of 10-8 atm. cm³/s minimum. The Adapters use fused in glass

seals between center contact and outer



conductor. This ensures complete hermeticity of the units. The adapters are normally used at vacuum chambers testing products that

are intended for outer space with the testing equipment and the personnel staying at regular environment. Available connector styles are 1.85 mm, 2.4 mm, 2.92 mm, N and TNC.

www.spectrum-et.org

Remcom

Stand 282

WaveFarer™ Automotive Radar **Simulation Software**



WaveFarer is a targeted software solution that simulates raw radar returns for drive test

scenarios. High fidelity simulations predict scattered returns from a scene, with support for frequencies up to and beyond 79 GHz. Near-field propagation methods compute raw radar returns from target objects while considering multipath from

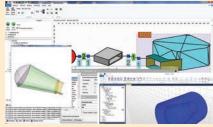
ground reflections. WaveFarer enables OEMs and Tier 1 suppliers to virtually test and refine results earlier in the design process, improving installed sensor performance.

www.remcom.com

Mician GmbH

Stand 287

µWave Wizard Hybrid EDA Software Tools



Mician, a developer of EM software tools for the analysis, synthesis and optimization of passive components like feeding networks, couplers, multiplexers and horn antennas, including reflectors, will show their µWave Wizard hybrid EDA software tools. The tools combine the flexibility of fast and powerful numerical methods with an appealing and ergonomic GUI that enables flexibility and openness including CAD export formats interfacing with most mechanical design tools.

www.mician.com

Teledyne Relays

Stand 299

Indium Phosphide HEMT RF Switch



Teledyne Relays introduces the InP1012-40, a new indium phosphide HEMT RF switch. This SPDT reflective switch has a 10 kHz to 40 GHz bandwidth, low

insertion loss, high linearity and a switching time under 100 ns. The InP1012-40 can operate from -65°C to 125°C, tolerate up to 100 krads of radiation and its 9 mm³ sized flip-chip packaging provides shock and vibration resistance. These features make this RF switch perfect for military and space applications, ATE systems and RF and microwave communication.

www.teledynerelays.com

Passive Plus Inc.

Stand 308

Capacitors



Passive Plus Inc. (PPI) is now offering the 0708N (0.065 in. × 0.080 in.) series capacitor. With vertical electrodes which increase

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Stand 321

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www.arww-rfmicro.com/html/ps-dual-bandamplifiers.asp

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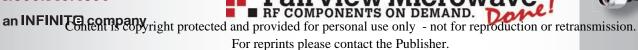




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Software and Hardware Near-Field Transformations for 5G OTA Testing

Benoît Derat, Corbett Rowell, Adam Tankielun and Sebastian Schmitz Rohde & Schwarz, Munich, Germany

Increased capacity in 5G mobile communications requires rolling out massive MIMO base stations with network and mobile terminals at both sub-6 GHz and mmWave frequencies. Dynamic beamforming and the absence of RF test ports on the devices being tested make over-the-air (OTA) measurement pivotal to 5G deployment. Fortunately, OTA testing solutions employing software and hardware near-field transformations are meeting the challenges.

G new radio (NR) communication systems will increase the capacity of mobile radio networks using frequency bands in the sub-6 GHz region, called frequency range 1 (FR1) by 3GPP, and the mmWave range (FR2). New technological approaches selected by the industry and 3GPP promise greater bandwidth at lower operational expense.

In FR1, the main innovation effort is focused on the base station, with the enabling of massive MIMO techniques. ¹ 4G systems use single-user MIMO, where the user equipment (UE) calculates the inverse channel matrix to extract separate data streams. ⁵G multi-user MIMO (MU-MIMO) shifts the complexity from UEs to the base station by using a pre-coding matrix. Here, each data stream is received independently by separate receivers. Beamforming with antenna arrays of 64 to 512 elements reduces inter-

ference to adjacent users using MU-MIMO. In addition to facilitating the adoption of MU-MIMO to increase capacity, beamforming has other advantages. Its lower energy consumption brings a reduction in overall network operating costs by targeting individual UEs with their assigned signals.

Communication systems in the FR2 range use large available bandwidths at frequencies around 28 and 39 GHz. The impact is more than 60 dB path loss at 1 m distance and large electromagnetic field absorption in nearby objects. As with FR1 systems, the solution is to employ antenna arrays and beam steering, improving the gain on both the mobile device and base station sides of the network.

Whether for FR1 or FR2, 5G deployment relies on the performance of highly integrated solutions combining modem, RF front-end and antenna. The challenge

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is to define new methods and setups for performance evaluation, as RF test ports tend to disappear and beam steering technologies require system-level testing. In this context, both antenna and transceiver performance criteria must be measured OTA: effective isotropic radiated power (EIRP), total radiated power (TRP), effective isotropic sensitivity (EIS), total isotropic sensitivity (TIS), error vector magnitude (EVM), adjacent channel leakage ratio (ACLR) and spectrum emission mask (SEM). Assessing these OTA raises the critical question of the required measurement distance. Antenna characteristics are usually measured in the far field. Using direct far-field probing and applying the Fraunhofer distance criterion (R = $2D^2/\lambda$), a 75 cm massive MIMO device under test (DUT) radiating at 2.4 GHz should be evaluated in a chamber with at least 9 m range length. Even a 15 cm smartphone transmitting at 43.5 GHz needs a 6.5 m testing distance. This distance is required to create a region encompassing the

DUT where the impinging field is as uniform as possible and approaches a plane wave with phase deviation below 22.5 degrees, known as the quiet zone.

Research shows that actual farfield behavior in the peak directivity region can start much closer than the Fraunhofer distance.² These results proved, for example, that the far-field EIRP or EIS of a 15 cm DUT radiating at 24 GHz can be assessed at a distance as short as 1.14 m. Distance reduction of about 70 percent comes at the price of increased longitudinal taper error, caused by the deviation of the apparent phase center from the center of the measurement coordinate system. Also, sidelobe levels cannot be evaluated accurately at shorter distances.³ While direct far-field measurements at shorter distances are not convenient for all applications, there is an incentive to do so when conditions of application are verified. This is because large OTA anechoic chambers have high costs of ownership and limited dynamic range. Typical applications may be in the "white box" case, where the antenna location within the device and its aperture size are known.

NEAR-FIELD TO FAR-FIELD

Direct far-field measurements under "white box" assumptions may be inappropriate when the radiation aperture is larger than the quiet zone, the antenna cannot be precisely identified within the DUT or multiple antennas transmit simultaneously, e.g., from two extreme edges of a DUT which does not fit within the quiet zone. The "black box" scenario must then be considered, where the radiating currents can flow anywhere within the DUT. A first efficient approach to treat such cases in a compact environment is to employ software near-field to far-field transformations (NF-FF), for which the quiet zone size question becomes irrelevant. Mathematical implementations of NF-FF may vary, but the concept is generally the same: at least two polarization components of the electromagnetic field (E, H or a mixture of the two) are measured in magnitude and phase over a surface encompassing the DUT. The measured data is processed using functions to propagate the fields toward larger distances and extract far-field radiation components. From the Huygens principle, the knowledge of two phasors is enough to reconstruct exactly all six field components outside the surface. Alternative transformation methods use spherical wave expansion, plane wave expansion or integral equation resolution, with techniques to improve computational efficiency or accuracy by taking parameters such as spatial sampling rate, scanning area or truncation into account.

Figure 1 shows a commercial system capable of both direct far-field and near-field measurements with spherical scanning around the DUT using a conical cut positioner. On this system, the DUT is positioned on a turntable rotating in azimuth, while a dual-polarized Vivaldi antenna is mounted at the tip of a boom rotating in elevation. An RF test port available at the DUT connects one port of a vector network analyzer (VNA); the measurement antenna





MMIC Selection Guide



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CMD283C3 2 to 6 GHz

Ultra Low Noise Amplifier

| Gain27 dB |
|--------------------------------------|
| Noise Figure |
| Output P1dB |
| Output Psat |
| OIP3 |
| Bias Voltage Vdd/Vgg +2 to +5/+1.5 V |
| Bias Current |



CMD215 DC to 40 GHz

SPDT Reflective Switch

| Insertion Loss. 2.3 dB |
|------------------------|
| Isolation |
| Input P1dB |
| Return Loss |
| Switch Speed4 ns |
| Control Voltage 0/-5 V |



CMD280 DC to 30 GHz

Digital Attenuator

| Number of Bits5 |
|-----------------------|
| Insert. Loss |
| Attn Range |
| Input P0.1dB |
| Input IP3 |
| Control Voltage0/-5 V |



CMD240P4 DC to 22 GHz

Distributed Amplifier

| Gain |
|------------------------------|
| Noise Figure |
| Output P1dB |
| Output Psat |
| OIP3 |
| Bias Voltage+5 to +8/-0.65 V |

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Low Noise Amplifiers (LNAs)

| Part Number | Frequency (GHz) | Gain (dB) | Noise Figure (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|----------------|--------------------|--------------|-------------------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD228 | 2-6 | 30 | 1.2 | 12 | 14 | 23 | 3-5 / 3-5 | 45 | DIE |
| CMD283C3 | 2-6 | 27 | 0.6 | 16 | 18 | 26 | 2-5 | 42 | 3x3 QFN |
| CMD228P4 | 2 - 6 | 28 | 1.5 | 13 | 14 | 25 | 3-5 / 3-5 | 45 | 4x4 QFN |
| CMD276C4 (GaN) | 2.6 - 4 | 14.5 | 1.2 | 25.5 | 28 | 32 | 5-28 / -1.5 | 225 | 4x4 QFN |
| CMD185 | 4 - 8 | 15.5 | 1.9 | 15 | 17 | 29 | 2-5 | 75 | DIE |
| CMD185P3 | 4 - 8 | 15.5 | 1.9 | 15 | 17 | 29 | 2-5 | 75 | 3x3 QFN |
| CMD270 | 4 - 8 | 15.5 | 1.8 | 16 | 17 | 30 | 2-5 | 60 | DIE |
| CMD270P3 | 4 - 8 | 15.5 | 1.8 | 16 | 17 | 30 | 2-5 | 60 | 3x3 QFN |
| CMD219 (GaN) | 4 - 8 | 23 | 1.0 | 18 | 26 | 28 | 5-28 / -2.3 | 75 | DIE |
| CMD219C4 (GaN) | 4 - 8 | 22.5 | 1.0 | 17 | 25.5 | 28 | 5-28 / -2.3 | 75 | 4x4 QFN |
| CMD277C4 (GaN) | 5 - 7 | 20 | 1.2 | 26.5 | 29.5 | 33.5 | 5-28 / -1.5 | 200 | 4x4 QFN |
| CMD119P3 | 5 - 9 | 22 | 1.2 | 11 | 13 | 21 | 2-4.5 | 30 | 3x3 QFN |
| CMD218 (GaN) | 5 - 9 | 22 | 1.1 | 21.5 | 26 | 30 | 5-28 / -2.7 | 80 | DIE |
| CMD229 | 5 - 11 | 27 | 1.4 | 13 | 15 | 25 | 3-5 / 3-5 | 45 | DIE |
| CMD229P4 | 5 - 11 | 26 | 1.5 | 13 | 15 | 24 | 3-5 / 3-5 | 45 | 4x4 QFN |
| CMD132 | 5 - 11 | 23 | 1.4 | 10 | 13 | 22 | 2-4.5 | 30 | DIE |
| CMD132P3 | 5 - 11 | 21 | 1.4 | 10 | 13 | 22 | 2-4.5 | 30 | 3x3 QFN |
| CMD263 | 5 - 11 | 23 | 1.4 | 11 | 15 | 23 | 2-4.5 | 35 | DIE |
| CMD263P3 | 5 - 11 | 22 | 1.4 | 11 | 15 | 21 | 2-4.5 | 35 | 3x3 QFN |
| CMD222 | 5 - 11 | 22 | 1.2 | 11 | 14 | 23 | 2-5 | 107 | DIE |
| CMD186P3 | 6 - 11 | 18.5 | 2.1 | 17 | 20 | 28 | 2-5 | 78 | 3x3 QFN |
| CMD157 | 6 - 18 | 26 | 1.5 | 11 | 13.5 | 23 | 2-4.5 | 52 | DIE |
| CMD157P3 | 6 - 18 | 26 | 1.5 | 11 | 13.5 | 23 | 2-4.5 | 52 | 3x3 QFN |
| CMD264 | 6 - 18 | 26 | 1.5 | 13 | 15 | 27 | 2-4.5 | 63 | DIE |
| CMD264P3 | 6 - 18 | 26 | 1.7 | 13 | 15 | 24 | 2-4.5 | 63 | 3x3 QFN |
| CMD194 | 6 - 20 | 20 | 2.0 | 15.5 | 16.5 | 26 | 2-5 | 120 | DIE |
| CMD194C3 | 6 - 20 | 20 | 2.0 | 15.5 | 16.5 | 26 | 2-5 | 120 | 3x3 QFN |
| CMD278C4 (GaN) | 8 - 12 | 15 | 1.8 | 28 | 30 | 33 | 5-28 / -1.5 | 280 | 4x4 QFN |
| CMD167P3 | 8 - 16 | 16 | 1.8 | 11 | 13 | 23 | 2-4 | 50 | 3x3 QFN |
| CMD223 | 9 - 18 | 22 | 1.5 | 13.5 | 16 | 22.5 | 3-5 | 93 | DIE |
| CMD161 | 10 - 14 | 19 | 1.05 | 5 | 12 | | 2-4 / 1.5 | 20 | DIE |
| CMD189P3 | 10 - 14 | 19 | 1.4 | 4 | 7 | 13 | 1-4 / 1.5 | 20 | 3x3 QFN |
| CMD159 | 10 - 17 | 26 | 1.1 | 4 | 10 | 14 | 2-4 / 1.5 | 29 | DIE |
| CMD167 | 10 - 17 | 15 | 2.0 | 11 | 13 | 24 | 2-4 | 55 | DIE |
| CMD224 | 16 - 26 | 23 | 2.2 | 7 | 13 | 18 | 2-5 | 110 | DIE |
| CMD160 | 17 - 25 | 26.5 | 1.4 | 8 | 11 | 16 | 2-4 / 1.5 | 26 | DIE |
| CMD160C4 | 17 - 25 | 26.5 | 1.6 | 8 | 11 | 16 | 2-4 / 1.5 | 26 | 4x4 QFN |
| CMD163 | 17 - 27 | 24 | 1.3 | 19 | 20 | 26 | 2-4/3 | 120 | DIE |
| CMD163C4 | 17 - 27 | 23 | 1.7 | 18 | 19 | 26 | 2-4/3 | 120 | 4x4 QFN |
| CMD162 | 26 - 34 | 22 | 1.7 | 7 | 9 | 14 | 1-4 | 25 | DIE |
| CMD188 | 26 - 34 | 20 | 1.4 | 6 | 8 | 15 | 1-4/2 | 20 | DIE |
| CMD190 | 33 - 45 | 19 | 2.1 | 4 | 7 | 13 | 1-4/2 | 25 | DIE |

Low Phase Noise Amplifiers (LPNAs)

| Part Number | Frequency (GHz) | Phase Noise (dBc/Hz @ 10kHz) | Gain (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|-------------|--------------------|------------------------------------|--------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD245 | 6 - 18 | -165 | 18 | 18 | 22 | 29 | 3-5/3 | 76 | DIE |
| CMD245C4 | 6 - 18 | -165 | 18 | 18 | 22 | 29 | 3-5/3 | 76 | 4x4 QFN |
| CMD274P4 | 2 - 20 | -165 | 17 | 19 | 22 | 30 | 5/3 | 86 | 4x4 QFN |
| CMD246 | 8 - 22 | -165 | 17 | 13 | 18 | 25 | 3-5/3 | 48 | DIE |
| CMD246C4 | 8 - 22 | -165 | 17 | 13 | 18 | 25 | 3-5/3 | 48 | 4x4 QFN |
| CMD275P4 | DC - 26.5 | -165 | 16 | 18 | 20.5 | 29 | 5/3 | 74 | 4x4 QFN |
| CMD247 | 30 - 40 | <-160 | 13 | 13.5 | 15 | 21 | 2-4 / 2-3 | 28 | DIE |

NEW PRODUCT

Distributed Amplifiers

| Part Number | Frequency (GHz) | Gain (dB) | Noise Figure (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|-------------|--------------------|--------------|-------------------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD173 | DC - 20 | 15 | 2 | 18 | 20 | 28 | 5-8/3 | 78 | DIE |
| CMD173P4 | DC - 20 | 15 | 2 | 18 | 20 | 28 | 5-8/3 | 78 | 4x4 QFN |
| CMD192 | DC - 20 | 19.5 | 1.9 | 24.5 | 26 | 31 | 5-8 / -1 | 200 | DIE |
| CMD192C5 | DC - 20 | 19.5 | 1.9 | 24.5 | 26 | 31 | 5-8 / -1 | 200 | 5x5 QFN |
| CMD201 | DC - 20 | 12 | 3.4 | 29 | 30 | 38 | 10/-0.5/5 | 400 | DIE |
| CMD201P5 | DC - 20 | 11 | 3.4 | 27 | 30 | 38 | 10/-0.5/5 | 400 | 5x5 QFN |
| CMD249 | DC - 20 | 13 | 3.4 | 30 | 31 | 38 | 10/-0.95 | 400 | DIE |
| CMD249P5 | DC - 20 | 13 | 3.4 | 30 | 31 | 38 | 10/-0.95 | 400 | 5x5 QFN |
| CMD233 | 2 - 20 | 9 | 4.5 | 20.5 | 22 | 24 | 3-6 | 120 | DIE |
| CMD233C4 | 2 - 20 | 9 | 4.5 | 20.5 | 22 | 24 | 3-6 | 120 | 4x4 QFN |
| CMD238 | 2 - 20 | 14 | 4.5 | 26 | 27 | 34 | 5-8 | 360 | DIE |
| CMD241 | 2 - 22 | 13.5 | 2.3 | 21 | 23 | 28 | 5-8/-0.65 | 74 | DIE |
| CMD241P4 | 2 - 22 | 13.5 | 2.3 | 21 | 23 | 28 | 5-8/-0.65 | 74 | 4x4 QFN |
| CMD197 | 1 - 24 | 16 | 2.5 | 22 | 24 | 32 | 5-8 | 225 | DIE |
| CMD197C4 | 1 - 24 | 16 | 2.5 | 24 | 25 | 31 | 5-8 | 225 | 4x4 QFN |
| CMD240 | DC - 22 | 15 | 2.2 | 19 | 22 | 28 | 5-8/-0.65 | 80 | DIE |
| CMD240P4 | DC - 22 | 15 | 2.2 | 19 | 22 | 28 | 5-8/-0.65 | 80 | 4x4 QFN |
| CMD244 | DC - 24 | 18 | 2.5 | 25 | 26.5 | 32 | 5-8 / -0.65 | 185 | DIE |
| CMD242 | DC - 40 | 11 | 4.4 | 18 | 21 | 27 | 5-8 / -0.32 | 100 | DIE |
| CMD206 | DC - 50 | 11 | 3.5 | 12 | 14.5 | 22 | 4/3 | 32 | DIE |

NEW PRODUCT

Driver Amplifiers

| Part Number | Frequency (GHz) | Gain (dB) | Noise Figure (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|-------------|--------------------|--------------|-------------------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD231 | 2 - 6 | 14.5 | 4.5 | 13.5 | 16.5 | 23.5 | 3-8 | 45 | DIE |
| CMD231C3 | 2 - 6 | 14.5 | 4.5 | 13.5 | 16.5 | 23.5 | 3-8 | 45 | 3x3 QFN |
| CMD232 | 2 - 9 | 15 | 4.5 | 17 | 18.5 | 23 | 5-6 | 90 | DIE |
| CMD232C3 | 2 - 9 | 15 | 4.5 | 17 | 18.5 | 23 | 5-6 | 90 | 3x3 QFN |
| CMD191C4 | 4 - 10 | 20 | 4.5 | 21.5 | 22.5 | 30 | 5 | 123 | 4x4 QFN |
| CMD158 | 6 - 16 | 20 | 3.5 | 20 | 21 | 26 | 3-6 | 95 | DIE |
| CMD158P3 | 6 - 14 | 19.5 | 4 | 19.5 | 20.5 | 26.5 | 3-6 | 95 | 3x3 QFN |
| CMD158C4 | 6 - 16 | 21 | 4 | 20 | 21 | 26 | 3-6 | 95 | 4x4 QFN |

Driver Amplifiers Continued

| Part Number | Frequency (GHz) | Gain (dB) | Noise Figure (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|-------------|--------------------|--------------|-------------------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD200 | 9 - 13 | 15.5 | 3.25 | 15.5 | 17 | 20.5 | 5 | 38 | DIE |
| CMD187 | 2 - 20 | 22.5 | 6 | 14 | 16 | 29 | 3/2 | 115 | DIE |
| CMD187C4 | 2 - 20 | 22.5 | 6 | 13 | 16 | 29 | 3/2 | 115 | 4x4 QFN |
| CMD166 | 20 - 40 | 9 | 4.5 | 17 | 18 | 27 | 2-4 | 76 | DIE |
| CMD207 | 20 - 40 | 35 | 5.5 | 18.5 | 21 | 29 | 4/3 | 270 | DIE |
| CMD199 | 26 - 35 | 15 | 3.5 | 19.5 | 21.5 | 24.5 | 5 | 72 | DIE |
| CMD243 | 26 - 35 | 15.5 | 4.4 | 21 | 22.5 | 26 | 3-5 | 90 | DIE |

NEW PRODUCT

Power Amplifiers (PAs)

| Part Number | Frequency (GHz) | Gain (dB) | Noise Figure (dB) | Output P1dB (dBm) | Output Psat (dBm) | OIP3 (dBm) | Bias Voltage (V) | Bias Current (mA) | Package |
|--------------|--------------------|--------------|-------------------------|-------------------------|-------------------------|---------------|------------------------|-------------------------|---------|
| CMD169P4 | 5 - 7 | 19 | 6.5 | 28.4 | 29.4 | 37 | 7/3 | 375 | 4x4 QFN |
| CMD170P4 | 7.5 - 9 | 30 | 6.5 | 28.3 | 29 | 34 | 7/3 | 365 | 4x4 QFN |
| CMD171P4 | 9.5 - 11 | 21 | 6.5 | 28.4 | 29 | 35 | 7/3 | 380 | 4x4 QFN |
| CMD216 (GaN) | 14 - 18 | 16 | | 37 | 38 | 43 | 28 / -3.4 | 550 | DIE |
| CMD262 (GaN) | 26 - 28 | 26 | | 37.5 | 38.5 | | 28 / -4 | 400 | DIE |
| CMD217 (GaN) | 28 - 32 | 20 | | 36.7 | 39.3 | 41 | 28 / -3.4 | 580 | DIE |
| CMD184 (GaN) | 0.5 - 20 | 13 | | 34.5 | 36.5 | 42 | 28 /-2.8/10 | 700 | DIE |
| CMD201 | DC - 20 | 12 | 3.4 | 29 | 30 | 38 | 10/-0.5/5 | 400 | DIE |
| CMD201P5 | DC - 20 | 12 | 3.4 | 27 | 30 | 38 | 10/-0.5/5 | 400 | 5x5 QFN |
| CMD249 | DC - 20 | 13 | 3.4 | 30 | 31 | 38 | 10/-0.95 | 400 | DIE |
| CMD249P5 | DC - 20 | 13 | 3.4 | 30 | 31 | 38 | 10/-0.95 | 400 | 5x5 QFN |

NEW PRODUCT

Voltage Variable Attenuators

| Part Number | Frequency (GHz) | Insertion Loss (dB) | Attn Range (dB) | Input P1dB (dBm) | Input IP3 (dBm) | Return Loss (dB) | Control Voltage (V) | Max. Power (dBm) | Package |
|-------------|--------------------|---------------------------|-----------------------|------------------------|-----------------------|------------------------|---------------------------|------------------------|---------|
| CMD172 | 18 - 40 | 1.6 | 37 | 15 | 25 | 12 | 0/-3 | 30 | DIE |

NEW PRODUCT

Digital Attenuators

| Part Number | Frequency (GHz) | Insertion Loss (dB) | Attn Range (dB) | Input P0.1dB (dBm) | Return Loss (dB) | Control Voltage (V) | Number of Bits | Package |
|-------------|--------------------|------------------------|--------------------|--------------------------|------------------------|---------------------------|-------------------|---------|
| CMD279 | 2 - 30 | 3.5 | 15.5 | 27 | 42 | 0/+5 | 5 | DIE |
| CMD279C3 | 2 - 18 | 3.5 | 15.5 | 27 | 42 | 0/+5 | 5 | 3x3 QFN |
| CMD280 | DC - 30 | 3 | 15.5 | 24 | 42 | 0/-5 | 5 | DIE |
| CMD280C3 | DC - 18 | 3 | 15.5 | 24 | 42 | 0/-5 | 5 | 3x3 QFN |
| CMD281 | DC - 40 | 1.2 | 6 | 28 | 42 | 0/-5 | 2 | DIE |
| CMD281C3 | DC - 18 | 1.2 | 6 | 28 | 42 | 0 / -5 | 2 | 3x3 QFN |
| CMD282 | DC - 40 | 1.5 | 12 | 23 | 42 | 0/-5 | 2 | DIE |
| CMD282C3 | DC - 18 | 1.5 | 12 | 23 | 42 | 0/-5 | 2 | 3x3 QFN |

Switches (Non-Reflective)

| Part Number | Part Description | Frequency (GHz) | Insertion Loss (dB) | Isolation (dB) | Input P1dB (dBm) | Return Loss (dB) | Switch Speed (nS) | Control Voltage (V) | Package |
|-------------|---------------------|--------------------|---------------------------|-------------------|------------------------|------------------------|-------------------------|---------------------------|---------|
| CMD272P3 | DPDT | DC - 10 | 1 | 43 | 25 | 14 | 4 | 0/ +5 | 3x3 QFN |
| CMD273P3 | DPDT | DC - 12 | 1.7 | 42 | 25 | 13 | 12 | 0/ +5 | 3x3 QFN |
| CMD204 | SPST | DC - 20 | 1 | 50 | 25 | 17 | 1.8 | 0/-5 | DIE |
| CMD204C3 | SPST | DC - 20 | 1.3 | 48 | 25 | 15 | 1.8 | 0/-5 | 3x3 QFN |
| CMD230 | SPDT (refl) | DC - 26 | 1.4 | 40 | 21 | 16 | 3.4 | 0/-5 | DIE |
| CMD195C3 | SPDT | DC - 18 | 2 | 37 | 25 | 13 | 1.8 | 0/-5 | 3x3 QFN |
| CMD196C3 | SPDT | DC - 18 | 1.5 | 46 | 23 | 17 | 1.8 | 0/-5 | 3x3 QFN |
| CMD195 | SPDT | DC - 20 | 2 | 41 | 25 | 17 | 1.8 | 0/-5 | DIE |
| CMD196 | SPDT | DC - 28 | 1.75 | 46 | 23 | 15 | 1.8 | 0/-5 | DIE |
| CMD234C4 | SP3T | DC - 15 | 2 | 40 | 21 | 9 | 66 | 0/-5 | 4x4 QFN |
| CMD203 | SP4T | DC - 20 | 2.4 | 39 | 21 | 9 | 66 | 0/-5 | DIE |
| CMD203C4 | SP4T | DC - 20 | 2.4 | 39 | 21 | 9 | 66 | 0/-5 | 4x4 QFN |
| CMD235C4 | SP5T | DC - 18 | 2.5 | 40 | 21 | 9 | 66 | 0/-5 | 4x4 QFN |
| CMD236C4 | SP6T | DC - 18 | 2.5 | 42 | 18 | 9 | 60 | 0/-5 | 4x4 QFN |
| CMD215 | SPDT (refl) | DC - 40 | 2.3 | 36 | 19 | 16 | 4 | 0/-5 | DIE |

NEW PRODUCT Mixers

| MENT HODGET | | | | | | | | | | | |
|-------------|---------------------|------------------------|-------------------|-------------------|-------------------------|----------------------------|----------------------------|--------------------|---------|--|--|
| Part Number | Part Description | Freq. LO / RF (GHz) | Freq. IF (GHz) | LO Drive (dBm) | Conver. Gain (dB) | LO-RF Isolation (dB) | LO-IF Isolation (dB) | Input IP3 (dBm) | Package | | |
| CMD251C3 | Fund. Mixer | 4 - 8.5 | DC - 2.2 | +17 | -7 | 45 | 36 | 21 | 3x3 QFN | | |
| CMD252C4 | I/Q / IRM | 4 - 8 | DC - 2.4 | +20 | -6.5 | 52 | 27 | 25 | 4x4 QFN | | |
| CMD182 | I/Q / IRM | 6 - 10 | DC - 3.5 | +15 | -6 | 46 | 20 | 18 | DIE | | |
| CMD182C4 | I/Q / IRM | 6 - 10 | DC - 3.5 | +15 | -6 | 46 | 20 | 18 | 4x4 QFN | | |
| CMD257C4 | I/Q / IRM | 6 - 10 | DC - 3.5 | +21 | -5.5 | 40 | 18 | 25 | 4x4 QFN | | |
| CMD177 | Fund. Mixer | 6 - 14 | DC - 5 | +13 | -6.5 | 43 | 37 | 16 | DIE | | |
| CMD177C3 | Fund. Mixer | 6 - 14 | DC - 5 | +13 | -6.5 | 43 | 37 | 16 | 3x3 QFN | | |
| CMD253C3 | Fund. Mixer | 6 - 14 | DC - 5 | +19 | -6 | 43 | 39 | 23 | 3x3 QFN | | |
| CMD183C4 | I/Q / IRM | 7.5 - 13 | DC - 4.5 | +15 | -5.5 | 43 | 23 | 18 | 4x4 QFN | | |
| CMD258C4 | I/Q / IRM | 7.5 - 13 | DC - 3.5 | +21 | -5.5 | 38 | 20 | 25 | 4x4 QFN | | |
| CMD178C3 | Fund. Mixer | 11 - 21 | DC - 6 | +13 | -6 | 45 | 45 | 16 | 3x3 QFN | | |
| CMD254C3 | Fund. Mixer | 11 - 21 | DC - 6 | +19 | -6 | 48 | 44 | 22 | 3x3 QFN | | |
| CMD179 | Fund. Mixer | 16 - 26 | DC - 9 | +13 | -6.5 | 40 | 48 | 17 | DIE | | |
| CMD179C3 | Fund. Mixer | 16 - 26 | DC - 9 | +13 | -6.5 | 40 | 48 | 17 | 3x3 QFN | | |
| CMD255C3 | Fund. Mixer | 16 - 26 | DC - 9 | +19 | -6.5 | 40 | 33 | 24 | 3x3 QFN | | |
| CMD180 | Fund. Mixer | 20 - 32 | DC - 10 | +13 | -7 | 36 | 36 | 18 | DIE | | |
| CMD180C3 | Fund. Mixer | 20 - 32 | DC - 10 | +13 | -7 | 36 | 36 | 18 | 3x3 QFN | | |
| CMD181 | Fund. Mixer | 26 - 45 | DC - 12 | +17 | -6.5 | 37 | 29 | 22 | DIE | | |
| CMD261 | Fund. Mixer | 30 - 46 | 5 - 20 | +19 | -8 | 30 | 20 | 21 | DIE | | |

Multipliers

| Part Number | Part Description | Input Freq. (GHz) | Output Freq. (GHz) | Input Power (dBm) | Output Power (dBm) | Fo Isolation (dB) | 3 Fo Isolation (dB) | Package |
|-------------|-----------------------|-------------------------|--------------------------|-------------------------|--------------------------|-------------------------|---------------------------|---------|
| CMD225 | Passive Freq. Doubler | 4 - 8 | 8 - 16 | 15 | 3 | 48 | 50 | DIE |
| CMD225C3 | Passive Freq. Doubler | 4 - 8 | 8 - 16 | 15 | 3 | 48 | 50 | 3x3 QFN |
| CMD226 | Passive Freq. Doubler | 7 - 11 | 14 - 22 | 15 | 5 | 44 | 46 | DIE |
| CMD226C3 | Passive Freq. Doubler | 7 - 11 | 14 - 22 | 15 | 5 | 44 | 46 | 3x3 QFN |
| CMD227 | Passive Freq. Doubler | 8 - 15 | 16 - 30 | 15 | 4 | 40 | 43 | DIE |
| CMD227C3 | Passive Freq. Doubler | 8 - 15 | 16 - 30 | 15 | 4 | 40 | 43 | 3x3 QFN |
| CMD214 | Active Freq. Doubler | 12 - 18 | 24 - 36 | 13 | 17 | 32 | 25 | DIE |
| CMD213 | Active Freq. Doubler | 15 - 20 | 30 - 40 | 17 | 17 | 46 | | DIE |
| CMD256 | Passive Freq. Doubler | 14 - 20 | 28 - 40 | 15 | 0 | 38 | | DIE |

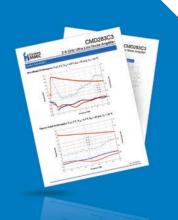
NEW PRODUCT

Phase Shifters

| Part Number | Frequency (GHz) | Number of Bits | Bit Resolu. (deg) | Insert. Loss (dB) | Return Loss (dB) | Phase Error (deg) | Input P1dB (dBm) | Input IP3 (dBm) | Package |
|-------------|--------------------|-------------------|-------------------------|-------------------------|------------------------|-------------------------|------------------------|-----------------------|---------|
| CMD175P4 | 2 - 4 | 5 | 11.25 | 7 | 17 | +/- 5 | 24 | 37 | 4x4 QFN |
| CMD174 | 3 - 6 | 5 | 11.25 | 7.6 | 15 | +/- 2 | 26 | 36 | DIE |
| CMD174P4 | 3 - 6 | 5 | 11.25 | 7.6 | 15 | +/- 2 | 26 | 36 | 4x4 QFN |
| CMD176P4 | 13 - 17 | 4 | 22.5 | 8 | 14 | +/- 5 | 26 | 41 | 4x4 QFN |







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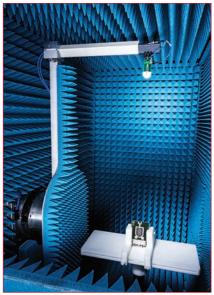
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TechnicalFeature



▲ Fig. 1 Spherical measurement system (ATS 1000), capable of near-field software transformation, measuring a 28 GHz array.

ports connect to two other terminals of the VNA, enabling near-field assessment through measurements of complex S-parameters.

Near-field measurement methods often rely on underlying as-

sumptions about passive or RF-fed antenna testing:

- The antenna feed port is accessible with a signal fed to the antenna that is used as a phase reference.
- The RF signal is a continuous wave signal.
- Reciprocity applies so that transmit (Tx) and receive (Rx) patterns at the same frequency are identical.

There are workarounds available in Tx cases where such assumptions do not apply. For example, techniques can address the case of a DUT transmitting a modulated signal with no access to the antenna feed port. Hardware and processing implementations to retrieve the propagation phase vary, for example using interferometric techniques or multi-port phase coherent receivers4 with the addition of a dedicated phase reference antenna. For systems like those in Figure 1, this antenna is typically attached to the azimuth turntable. Alternative approaches include phaseless methods when the phase information is retrieved from magnitude measurements.

However, the Rx mode is more complex. First, the reciprocity assumption does not apply to mobile phone and base station devices, as the Rx RF component chain is, in general, different from the Tx RF chain. For a DUT with no test port, the power available at the Rx input of the RF front-end generated by an impinging wave coming from the probe antenna (here used as the transmitter) cannot be straightforwardly predicted in the near field. In other words, it is not possible to isolate the intrinsic receiving properties of the DUT in the far field from near-field coupling effects resulting from the test setup. There is also no access to a phase reference, so the NF-FF software transformation becomes inapplicable. Therefore, EIRP can be evaluated accurately in the near-field using NF-FF software but not EIS.

TRANSCEIVER PERFORMANCE MEASUREMENTS

Another key question is the OTA evaluation of radio transceiver performance, such as EVM, ACLR or SEM. Software NF-FF approaches are designed for processing periodic portions of the RF signal (the carriers) that determine propagation. However, this part of the signal is of no interest to assess these performance parameters, so the challenge is to extract information from the carrier modulation.

The first difficulty is that these quantities depend strongly on the signal-to-noise ratio (SNR) at the receiver (a spectrum analyzer in the Tx mode or the DUT in the Rx mode). This can be overcome by first assessing the complete 3D Tx or Rx pattern to determine the peak direction. Demodulation and EVM or other measurements can then be conducted at this specific location. The guestion remains whether the obtained values are reliable and reflect the results obtained in the far field. In the case of a single transceiver, the near-field EVM must be the same as the far-field EVM so long as the SNR is above a certain threshold dependent on modulation scheme, e.g., better than

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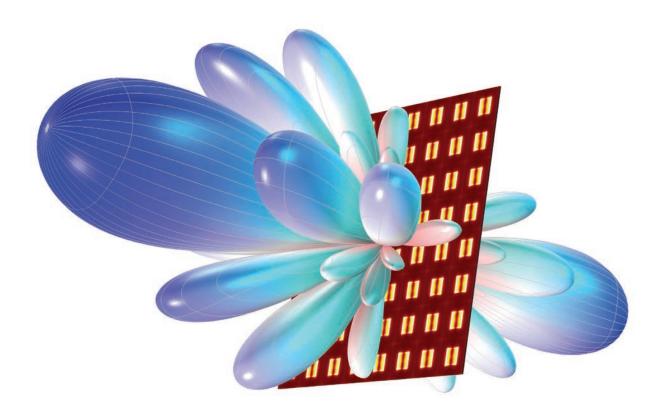


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20 dB. For multiple independent transceivers operating simultaneously, the near-field EVM may not be straightforwardly related to the far-field EVM because of positional dependence of the noise figure in the near field.

HARDWARE NEAR-FIELD TRANSFORMATIONS

Alternative testing methods enable OTA assessment in the near field without a software transformation, rather a hardware-based one. The idea is to physically create far-field conditions in a specified quiet zone region within a short range. This is known as "indirect far field." A compact antenna test range (CATR) uses a mirror to transform a spherical wave into a planar wave and vice-versa. Using Fermat's principle of least time, a planar wave can be focused on a single point using a parabolic mirror. If a measurement antenna is placed at this focal point, using the reciprocity principle, a plane wave can be generated as the parabolic mirror

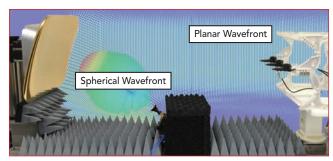


Fig. 2 Compact antenna test range with a roll-edge reflector collimating a spherical wavefront into a planar wavefront.

reflects a certain planar component of the incoming spherical wave from the measurement (or feed) antenna into the quiet zone where the DUT is placed (see Figure 2).

The error inside a CATR system comes from two main sources: the mirror geometry—the edge treatment and smoothness of the surface which limit the frequency rangeand the feed antenna characteristics. If the reflector is built with a simple parabolic section, the sharp edges cause diffraction, which significantly contaminates the quiet

smiths interconnect

zone by producing ripples as large as 2 dB. Techniques to mitigate this phenomenon clude serrations and rolled edges to scatter the energy away from the quiet zone. The size and shape of the serrated/rolled edges determine the lowest operat-

ing frequency, where the surface roughness determines the upper frequency. Feed antenna pattern characteristics have a direct impact on the size of the quiet zone, as the mirror essentially projects the radiation pattern of the feed antenna onto the quiet zone. The reflector size with serrated/rolled edges is generally at least 2× the DUT/quiet zone size, where a reflector with sharp edges is 3 to 4× the size of the quiet zone. The optimum reflector to DUT separation distance is (5/3)× the focal length of the reflector. An optimal focal length can be derived from the manufacturing shape tolerances with a range of roughly 0.3 to 1 for the ratio of focal length to parabolic diameter.

Since the quiet zone size is dependent on the reflector characteristics instead of range length, it is much easier to create a large quiet zone inside small enclosures. Figure 3 shows the measured magnitude quiet zone size of 27 cm at 28 GHz of a CATR, similar to the one shown



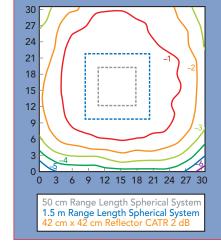


Fig. 3 28 GHz, 2 dB amplitude taper quiet zones for a roll-edge compact range system vs. direct far-field systems.

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in Figure 2, with a 42 cm × 42 cm reflector. This CATR setup fits within a chamber as small as 2 m × 1.5 m × 0.85 m. A direct far-field measurement system featuring the same quiet zone size would require a 14.5 m range.

Such technologies are of great interest for testing UEs or base stations operating in 5G NR FR2, promising a significant decrease in the size of test environments. In addition, CATR has the same capabilities as a far-field system, i.e., instantaneous and direct measurements of RF transceiver performance in both Tx and Rx. As the path loss of such a system only occurs between the limited region where waves propagate between the feed and the reflector, the dynamic range of a CATR system is better than a direct far-field approach. Using Figure 3 as an example, the CATR system has a

focal length of 0.7 m compared to the equivalent far-field range length of 14 m, resulting in a path loss difference of 26 dB.

PLANE WAVE SYNTHESIS

A CATR reflector is typically built using a solid piece of aluminum to maintain the strict surface geometry requirements. The 5G FR2 DUT size requirements allow for compact and rather light reflectors (20 to 40 kg). In the 5G FR1 range, reflector weight significantly increases, up to hundreds of kilograms for base station DUTs. The cost, fabrication time and handling of large heavy mirrors becomes prohibitive. A lightweight and cost-effective alternative is to use an "electronic version" of the CATR mirror.³ By combining the radiation of multiple antennas assembled in a phased array and fed with pre-determined signal magnitude and phase, a plane wave within a defined quiet zone is created. A version of this near-field focusing technique was used for several years for the measurement of large phased array radars at MIT Lincoln Labs and has been proposed as an OTA measurement baseline for base stations by 3GPP.5

Figure 4 shows the plane wave converting (PWC) system reported at the 2018 European Conference on Antennas and Propagation.³ It comprises an array of 156 wideband Vivaldi antennas with a beamforming network of phase shifters and attenuators, located at the rear. This PWC array is 1.8 m wide and creates a spherical quiet zone of 1 m diameter at a distance as short as 1.5 m in the frequency range from 2.3 to 3.8 GHz. In the setup of Figure 4, the DUT (here the calibration antenna) is mounted on a combined axis positioner, enabling full spheri-



Fig. 4 R&S PWC200 showing the PWC antenna array and calibration array mounted on a great-circle cut positioner.



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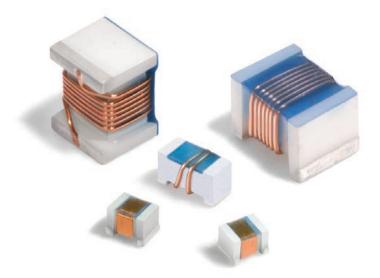
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Fig. 5 EVM of a single 20 MHz carrier measured using the R&S PWC200.

cal measurement. The calibration antenna is used for evaluating the appropriate compensations of the individual RF channels of the



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PWC array, as well as determining the path loss of the entire test system. The PWC system is reciprocal and has only one RF input/output which can either be connected to a signal generator, a spectrum analyzer or a VNA, enabling measurement of devices with or without RF test ports.

Figure 5 shows the single-carrier EVM measured with the PWC for an OFDM signal with five 20 MHz carriers in the range of 2.35 to 2.45 GHz, using a Rohde & Schwarz vector signal generator. The output power is 5 dBm and fed into a $60 \text{ cm} \times 60 \text{ cm}$ patch array DUT. The demodulation is carried out by a Rohde & Schwarz vector signal analyzer connected to the PWC, where the measurement span is 30.72 MHz. The EVM is as low as 0.41 percent, roughly corresponding to the internal EVM of the measurement instruments. EVM results were below 0.5 percent for the other four carriers, showing that the PWC adds negligible EVM to the measurement setup.

SUMMARY

Near-field techniques employing software transformations are suitable for evaluation of EIRP and TRP quantities. When Rx or demodulation is involved with a DUT using multiple non-identical RF transceivers, methods utilizing hardware field transformations such as CATR and PWC overcome the limitations of software NF-FF. They also provide compact and reliable alternatives to direct farfield measurements, making them well-suited for 3GPP RF conformance testing of UEs and base stations.

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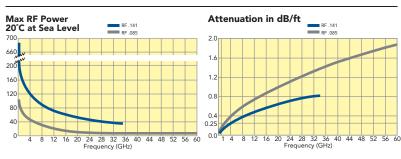
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he DPA is of interest for use in modern wireless communication networks to address the need for higher peak envelope power and better linearity. High efficiency is also desirable, but high efficiency with high linearity is difficult to achieve. Typical DPAs have high efficiency only at saturated output power. Efficiency is reduced at backed-off power levels to achieve the desired linearity. To improve linearity without reducing efficien-

cy, class F and inverse class F amplifiers are employed.¹ In addition, asymmetric DPAs using model-based nonlinear embedding² and optimized asymmetrical DPAs³ have been proposed. The real frequency technique is also used,⁴ as well as a tunable matching network⁵ using a fer-

roelectric capacitor for improving efficiency.

In this work, a new method to improve linearity employs a loaded capacitor CMRC structure. Because the CMRC exhibits a bandstop characteristic which can be used to reject undesired frequencies, it is used in the design of fourth subharmonic mixers.⁶ It has also been used to improve the performance of a class F power amplifier⁷ and a V-Band tripler.⁸ For these applications, however, the CMRC is used only for harmonic suppression; phase cannot be modified easily. In this work, not only are harmonics suppressed, but phase is flexibly modified. This makes it possible to improve the linearity of the DPA without reducing efficiency.

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Fig. 1 DPA using a tunable loaded capacitor CMRC.

DPA DESIGN

The architecture is shown in *Figure 1*. The signal of the peak (class C) amplifier passes through the CMRC and is combined with the

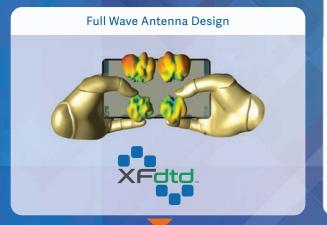
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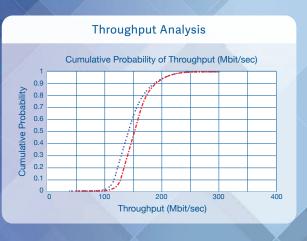


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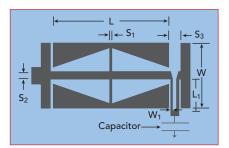
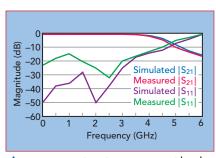


Fig. 2 Tunable loaded capacitor CMRC structure.

| TABLE 1 LOADED CAPACITOR CMRC VALUES | | | | | | |
|--------------------------------------|------------------------|----------|-----|--------------|--|--|
| L ₁ (mm) | W ₁ (mm) | D C (pF) | | Phase (°) | | |
| 8.2 | 0.5 | 0.4 | 0.8 | 89.1 | | |
| 8.2 | 0.3 | 0.4 | 1.2 | 88.7 | | |
| 8.4 | 0.3 | 0.4 | 1.3 | 106.3 | | |



ightharpoonup Fig. 3 Simulated vs. measured $|S_{21}|$ and $|S_{11}|$.

signal from the main (class AB) amplifier at the output. The $\lambda/4$ transmission line of the conventional DPA is replaced by the loaded capacitor CMRC, which performs the appropriate impedance transformation and phase delay offset. Because the peak amplifier operates class C, the main harmonic component and AM to PM distortion are generated at its output. Unlike a conventional DPA, however, the harmonic components are suppressed, while the AM to PM phase distortion of the peak amplifier can be corrected with a modified capacitor value in the CMRC.

The tunable loaded capacitor CMRC consists of the CMRC and a loaded capacitor coupled line (see Figure 2). The CMRC is a section of microstrip transmission line with an incorporated band gap structure. Its dimensions are L = 14.2 mm, W = $4.8 \text{ mm}, S_2 = 0.3 \text{ mm}, S_1 = 0.13 \text{ mm}$ and $S_3 = 2.2$ mm. The loaded capacitor coupled line has a length L₁ and a width W₁. The slot between

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Fig. 4 Tunable loaded capacitor

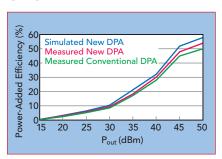


Fig. 5 Power-added efficiency of the new vs. conventional DPA.

the coupled lines (d) is 0.4 mm. Between the coupled line and ground is a tunable capacitor. The values of L_1 , W_1 and the loaded capacitor are listed in **Table 1** for several phases in the frequency range of 2570 to 2620 MHz.

Simulated and measured S-parameters of the CMRC are shown in Figure 3. In the frequency range of 0.5 to 3.75 GHz, the simulated and measured insertion loss are less than 0.5 dB and the simulated and measured return loss is greater than

FABRICATION AND MEASUREMENT

The DPA was fabricated on a Rogers 4350 substrate with a Freescale MRF8P26080H LDMOS transistor (see **Figure 4**). V_{DS} of the main and peak amplifiers was 28 V, while V_{GS} of main amplifier was 2.65 V and the V_{GS} of the peak amplifier was 2.28 V. The DPA was measured using a Keysight N9010A signal analyzer and E4438C vector signal

Simulated and measured PAE of the DPA using a CMRC are compared with the measured PAE of a conventional DPA in Figure 5. The maximum measured PAE of the new DPA is 54 percent at 2.6 GHz. Compared to the conventional DPA, the new DPA demonstrates an improvement of 5 to 6 percentage points.



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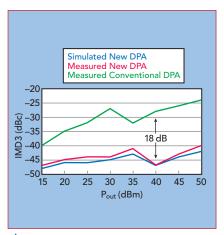


Fig. 6 IMD3 of the new vs. conventional DPA.

Figure 6 shows the simulated and measured IMD3 of the new DPA using a two-tone signal with a spacing of 5 MHz centered at 2.6 GHz. IMD3 is considerably improved compared to that of the conventional DPA due to the tuned loaded capacitor of the CMRC. The max IMD3 of the new DPA demonstrates an 18 dB improvement compared to a conventional DPA. Table 2 compares the performance of the new DPA design with several of the referenced works, showing that it simultaneously achieves low distortion and high PAE.

CONCLUSION

A novel, high linearity DPA uses a loaded capacitor CMRC structure to perform phase tuning and filtering. The harmonics and AM to PM distortion of the peak amplifier are suppressed, improving linearity compared to a conventional DPA, while preserving PAE.

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| TABLE 2 PERFORMANCE COMPARISON | | | | | | |
|--------------------------------|--------------------|----------------|-------------------|---------------------------|--|--|
| Reference | Frequency (GHz) | Max PAE (%) | Max IMD3 (dBc) | P _{out} (dBm) | Method | |
| 1 | 1 | 50.9 | -30 | 36 | Class F | |
| 3 | 1.92 to 2.17 | 53 | -50 | 48 | Asymmetric | |
| 4 | 2.2 to 2.96 | 60 | -30 | 40 | Broadband | |
| This Work | 2.57 to 2.62 | 54 | -50 | 50 | Tunable Loaded Capacitor CMRC | |





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Spatial Multiplexing for 5G Wireless Communications

Honglei Chen and Rick Gentile MathWorks, Natick, Mass.

ncreasing demand for higher data rates and channel capacity is driving the need to use the RF spectrum more efficiently. As a result, 5G wireless systems will use mmWave frequency bands to take advantage of the increased bandwidth. The higher operating frequencies enable large-scale antenna arrays, which can be used to mitigate severe propagation loss in the mmWave band. Large arrays can also be used to implement a MIMO system in which unique signals can be transmitted from different antenna elements in the array. MIMO systems enable spatial multiplexing techniques that can be used to improve data throughput.

The core idea of spatial multiplexing is to create multiple subchannels in scatterer-rich environments so that multiple data streams can be transmitted and recovered independently. This is achieved by applying a set of precoding and combining weights derived from the channel matrix. This concept is discussed first with an all-digital solution based on precoding in a MIMO-OFDM system that uses a spatial channel model. This channel model incorporates array pattern information to improve model fidelity.

Because 5G systems require large antenna arrays, applying digital weights on each antenna element is not always practical due to cost and space limitations. Hybrid beam-

forming techniques can be applied in a mixed RF and digital beamforming system to alleviate these restrictions. In a hybrid beamforming system, both the precoding weights and the combining weights are combinations of baseband digital weights and RF band analog weights. On the transmit side, the baseband digital weights modulate the incoming data streams to form input signals at each RF chain, and the analog weights then translate the signal at each RF chain to the signal radiated at each antenna element. The process is reversed on the receive side. This article includes an example with hybrid weights and compares the achieved spectral efficiency with the all-digital case.

SPATIAL MULTIPLEXING

The idea behind spatial multiplexing is that a MIMO system in a multipath channel with a rich scatterer environment can send multiple data streams simultaneously across the channel. For example, the channel matrix of a 4×4 MIMO channel becomes full rank because of the scatterers. This means that it is possible to send as many as four data streams at once. The goal of spatial multiplexing is less about increasing the signal-to-noise ratio (SNR) and more about increasing the information throughput.

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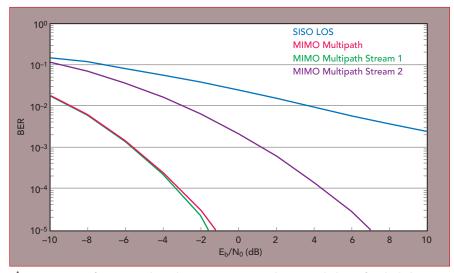
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▲ Fig. 1 BER of MIMO multipath streams compared to a single line-of-sight link.

The idea of spatial multiplexing is to separate the channel matrix into multiple modes so that the data stream sent from different elements in the transmit array can be independently recovered from the received signal. To achieve this, the data stream is precoded before the transmission and then combined after the reception. In the MATLAB models that follow, the precoding and combining weights can be computed from the channel matrix by:

[wp, wc] =
diagbfweights(mimompchan);

The information received by each receive array element is simply a scaled version of the trans-

mit array element, which results in multiple orthogonal subchannels within the original channel. The first subchannel corresponds to the dominant transmit and receive directions, so there is no loss in the diversity gain. In addition, it is possible to use other subchannels to carry information, as shown by the bit error rate (BER) curves in Figure 1, including the first two subchannels. The gain of the second data stream is not as high as the first stream, since it uses a less dominant subchannel. Still, the overall information throughput is improved. This concept will be applied to a MIMO-OFDM system

MIMO-OFDM SYSTEMS

MIMO-OFDM systems are common in wireless systems due to their robustness with frequency-selective channels and high data rates. With antenna arrays that implement spatial multiplexing, efficient techniques to realize the transmissions are necessary. As an example, consider an asymmetric MIMO-OFDM single-user system in which the maximum number of antenna elements on the transmit and receive ends are 1024 and 32, respectively, and up to 16 independent data streams. For clarity, a single link (one base station communicating with one mobile user) is modeled, but this structure could be extended for more complex configurations.

The link between the transmitter and receiver relies on channel sounding to generate the channel information needed for transmit beamforming. For a spatially multiplexed system, the availability of channel information at the transmitter allows for precoding to be applied to maximize the signal energy in the direction and channel of interest. Assuming a slowly varying channel, this process is facilitated by first sounding the channel with a reference transmission. The receiver then estimates the channel and feeds this information back to the transmitter, as shown in Figure 2. In this system, a preamble signal is first sent over all transmitting ele-

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EWDM-8G18G-65-70MV









DLVA-18G40G-42-50-CD-1

SDLVA-18G40G-65-CD-292FF

| PMI Model No. | FREQ Range (GHz) | TSS | Log Slope (mV/dB) | Dynamic Range Log (dBm) | Connector Type | Size (Inches) |
|---|------------------------|----------------|----------------------|-------------------------------|-------------------|-----------------------|
| EWDM-2G6G-65-70MV CW Immune http://www.pmi-rf.com/products-details/ ewdm-2g6g-65-70mv | 2 - 6 | -71 dBm Typ | 70 Nom | -65 to 0 | SMA | 4.2" x 2.9" x 0.8" |
| EWDM-2G8G-65-70MV CW Immune http://www.pmi-rf.com/products-details/ ewdm-2g8g-65-70mv | 2 - 8 | -71 dBm Max | 70 ± 3 | -65 to 0 | SMA | 2.82" x 2.25" x 0.5" |
| ERDLVA-2G8G-65-70MV CW Immune http://www.pmi-rf.com/products-details/ erdlva-2g8g-65-70mv | 2 - 8 | -71 dBm Typ | 70 ± 3 | -65 to 0 | SMA | 2.82" x 2.25" x 0.5" |
| EWDM-6G18G-65-70MV CW Immune http://www.pmi-rf.com/products-details/ ewdm-6g18g-65-70mv | 6 - 18 | -71 dBm Max | 70 Nom | -65 to 0 | SMA | 4.2" x 2.9" x 0.8" |
| EWDM-8G18G-65-70MV CW Immune http://www.pmi-rf.com/products-details/ ewdm-8g18g-65-70mv | 8 - 18 | -71 dBm Max | 70 ± 3 | -65 to 0 | SMA | 2.82" x 2.25" x 0.5" |
| ERDLVA-8G18G-65-70MV CW Immune http://www.pmi-rf.com/products-details/erdlva-8g18g-65-70mv | 8 - 18 | -71 dBm Max | 70 ± 3 | -65 to 0 | SMA | 2.82" x 2.25" x 0.5" |
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| DLVA-18G40G-42-50-CD-1 http://www.pmi-rf.com/products-details/ dlva-18g40g-42-50-cd-1 | 18 - 40 | -34 dBm Typ | 50 ± 3 | -32 to +10 | 2.92mm | 1.86" x 1.69" x 0.40" |
| SDLVA-18G40G-65-CD-292FF http://www.pmi-rf.com/products-details/ sdlva-18g40g-65-cd-292ff | 18 - 40 | -65 dBm Typ | 25 Nom | -63 to +2 | 2.92mm | 2.37" x 1.8" x 0.42" |



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ments. It is subsequently processed at the receiver after accounting for the channel effects. The receiver performs pre-amplification, OFDM demodulation, frequency domain channel estimation and calculation of the feedback weights based on channel diagonalization using singular value decomposition per data subcarrier. The specific system configuration is as follows:

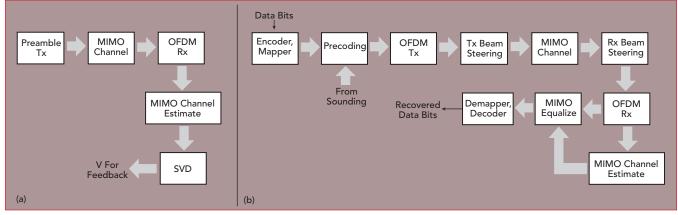
the array geometry of the transmitter and the beam patterns in azimuth and elevation. For simplicity, assume the steering angle is known with respect to the mobile location. In actual systems, the steering angle would be obtained from an angle-of-arrival estimation at the receiver, as a part of the channel sounding or initial beam tracking procedures.

A rectangular array at the transmitter is used, based on the desired number of data streams and transmit antennas. *Figure 3* shows

Multiple options exist for modeling spatial MIMO channels, typically selected based on the level of fidelity that is needed for the analysis.

For example, 5G channel models and the WINNER II channel models are spatially defined MIMO channels where the array geometry and location information can be specified. For this discussion, consider scattering-based channels with a single-bounce path through 100 scatterers placed randomly within a circle between the transmitter and receiver. The channel model allows path loss modeling and both lineof-sight (LOS) and non-LOS propagation conditions. For this analysis, a non-LOS propagation and isotropic antenna element pattern with linear geometry are configured. The same channel is used for both sounding and data transmission. The data transmission has a longer duration controlled by the number of data symbols.

The receive antenna array, shown in *Figure 4*, passes the propagated



▲ Fig. 2 Channel sounding (a) and data transmission/reception (b) flow.



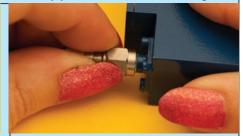
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2. Put your fingers firmly onto the knurls of the "Lock Nut".



3. Push "Lock Nut" forward and engage the Push-On end of the Adapter with the mating female. Back nut must be released.



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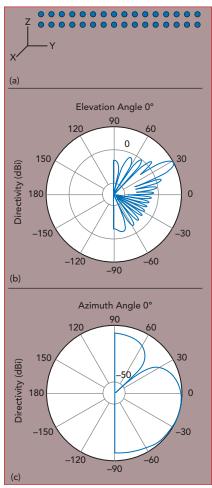


To unlock (when "Back Nut" is in unlocked mode) push the "Lock Nut" forward and stop reverse movement by



6. Keep fingers on "Back Nut" to ensure that "Lock Nut" cannot slide back and pull the connector off.

signal to the receiver to recover the original information embedded in the signal. Similar to the transmitter, the receiver used in a MIMO-OFDM



▲ Fig. 3 Transmitter array geometry (a) with azimuth (b) and elevation (c) beam patterns.

system contains many stages, including OFDM demodulator, MIMO equalizer, QAM demodulator and channel decoder. For this MIMO system, the displayed receive constellation of the equalized symbols offers a qualitative assessment of the reception. The actual BER offers the quantitative figure by comparing the actual transmitted bits with the received decoded bits (see *Figure 5*).

Parameters can be modified to vary the number of data streams, transmit/receive antenna elements, base station or array locations and

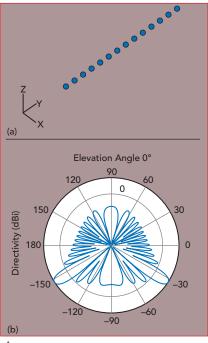
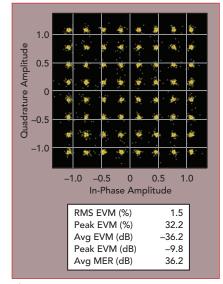


Fig. 4 Receiver array geometry (a) with azimuth beam pattern (b).

geometry, channel models and their configurations to study the parameters' individual or combined effects on the system. This framework can be used for further analysis but, so far, all of the precoding and combining were based on an all-digital system. As the antenna array size increases, an all-digital system may not be feasible, which leads to the use of hybrid beamforming.

HYBRID BEAMFORMING

In a hybrid beamforming system, both the precoding weights and the combining weights are combinations of baseband digital weights and RF band analog weights. This type of architecture is shown in *Figure 6*.

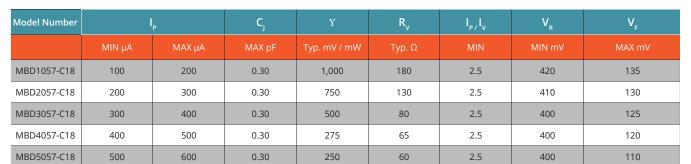


★ Fig. 5 Constellation diagram for the MIMO OFDM system.

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For this discussion, assume a set of larger arrays: The transmitter consists of a 64-element square array with four RF chains, and the receiver is based on a 16-element square array with four RF chains. Each antenna is connected to all RF chains, which means that each antenna is connected to four phase shifters. This type of array can be modeled by partitioning the array aperture into four completely connected subarrays. To maximize the spectral efficiency in the system, each RF chain can be used to send an independent data stream. In this case, the system supports up to four streams.

A scattering environment with six scattering clusters randomly distributed in space is used to define the channel. Within each cluster, there are eight closely located scatterers, for a total of 48 scatterers. The path gain for each scatterer is obtained from a complex circular symmetric Gaussian distribution.

As described earlier, in a spatial multiplexing system with all-digital beamforming, the signal is modulated by a set of precoding weights, propagated through the channel and recovered by a set of combining weights. Mathematically, this process can be described by Y = (X*F*H+N)*W where

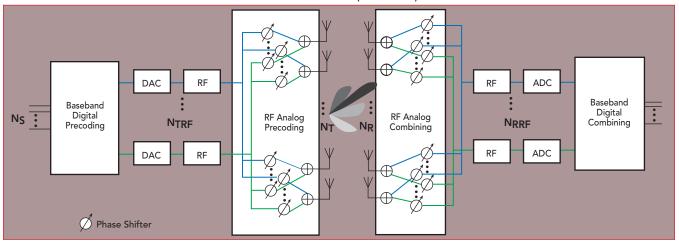


Fig. 6 Hybrid beamforming architecture.

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- Ns is the number of data streams.
- Nt is the number of transmit elements.
- Nr is the number of receive elements.
- Nrf is the number of RF channels.
- X is an Ns-column matrix whose columns are data streams.
- F is an Ns × Nt matrix representing the precoding weights.
- H is the channel representation.
- W is an Nr × Ns matrix representing the combining weights.
- N is an Nr-column matrix whose columns are the receiver noise at each element.
- Y is an Ns-column matrix whose columns are recovered data streams.

Since the goal of the system is to achieve better spectral efficiency, obtaining the precoding and combining weights can be considered an optimization problem in which the optimal precoding and combining weights make the product of F*H*W a diagonal matrix, so each data stream can be recovered independently.

In a hybrid beamforming system, the signal flow is similar. Both the precoding weights and the combining weights are combinations of baseband digital weights and RF band analog weights. The baseband digital weights convert the incoming data streams to input signals at each RF chain, and the analog weights then convert the signal at each RF chain to the signal radiated or collected at each antenna element. Note that the analog weights can only contain phase shifts. Mathematically, it can be written as F = Fbb*Frf and W = Wbb*Wrf, where

- Fbb is an Ns × NtRF matrix.
- Frf is an NtRF × Nt matrix.
- Wbb is an NrRF × Ns matrix.
- Wrf is an Nr × NrRF matrix.

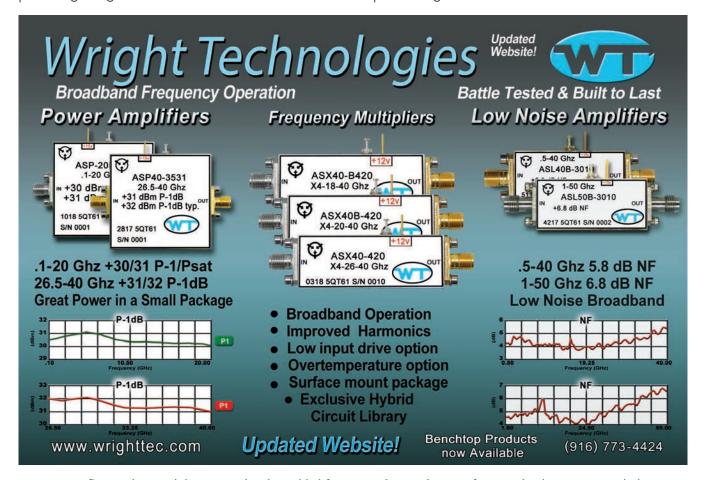
Since both Frf and Wrf can only be used to modify the signal phase, there are extra constraints on the optimization process to identify the optimal precoding and combining weights. Ideally, the resulting combination of Fbb*Frf and Wrf*Wbb are close approximations of F and W that are obtained without those constraints. Unfortunately, optimizing all four matrix variables simultaneously is quite difficult. Many algorithms exist that arrive at suboptimal weights

with a reasonable computational load. This example uses an approach that decouples the optimizations for the precoding and combining weights. It first uses the orthogonal matching pursuit algorithm to derive the precoding weights. The hybrid weights can be computed as

[Fbb, Frf] = helperHybridPrecoding
Weights(H, NtRF, Ns, At);

Once the precoding weights are computed, the result is used to obtain the corresponding combining weights. Assuming the channel is known, the unconstrained optimal precoding weights can be obtained by diagonalizing the channel matrix and extracting the first NtRF dominating modes.

The transmit beam pattern for both cases is shown in *Figure 7*. The response patterns show that even in a multipath environment, the number of dominant directions is limited. The beam pattern using the hybrid weights is similar to the beam pattern obtained using the optimal weights, especially for the dominant beams. This result means



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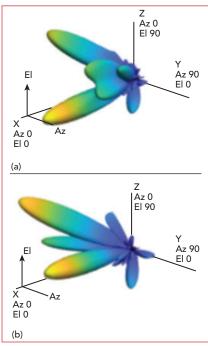
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▲ Fig. 7 Transmit patterns for all-digital (a) and hybrid (b) cases.

that the data streams can be successfully transmitted through those beams using hybrid weights.

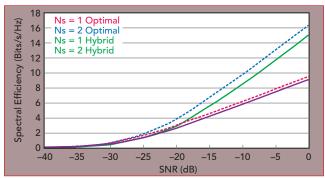


Fig. 8 Spectral efficiency of all-digital and hybrid systems.

One of the system-level performance metrics of a 5G system is the spectral efficiency. Figure 8 compares the spectral efficiency achieved using the optimal weights with the proposed hybrid beamforming weights. The simulation assumes one or two data streams. The transmit antenna array is assumed to be at a base station, with a focused beam coverage of 60 degrees in azimuth and 20 degrees in elevation. The signal can arrive at the receive array from any direction. The resulting spectral efficiency curve is obtained from 50 Monte Carlo trials for each SNR. Figure 8 shows that the spectral efficiency improves significantly by increasing the number of data streams. In addition, hybrid beamforming can perform close to what optimal weights can offer and uses less hardware.

SUMMARY

MIMO systems enable spatial multiplex-

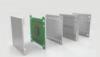
ing techniques that can be used to improve data throughput. This improvement is achieved by applying a set of precoding and combining weights derived from the channel matrix. Because 5G systems require large antenna arrays, applying digital weights on each antenna element is not always practical. Hybrid beamforming can be applied in a mixed RF and digital beamforming system to lower system costs. System modeling techniques can be used to explore system tradeoffs before any hardware is built, which can prevent costly errors and project delays.

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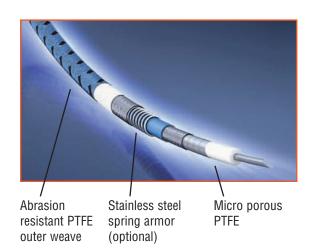
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Why V_{peak} is the Most Critical Aperture Tuner Parameter

Skyworks Solutions, Inc. *Irvine, Calif.*

here are multiple factors that designers of RF front-ends face. One of the most challenging is tuning an antenna for best performance. Good antenna design combined with aperture tuning enable wider bandwidth, increased data rates, lower power, longer battery life, smaller footprint and reduced bill of material cost. In this article, we discuss V_{peak}, or voltage handling, one of the most important antenna tuner parameters when choosing the right solution for antenna aperture tuning.

DEFINITIONS

Important definitions, specifications and other aspects to be considered in the design and selection of an antenna tuner include:

Total radiated power (TRP) is a measure of how much power is transmitted by an antenna, and **total isotropic sensitivity (TIS)** is a measure of an antenna system's receive sensitivity.

Aperture tuning changes the electrical length of an antenna to shift its resonance to the desired frequency band. Antenna aperture tuners improve the TRP and TIS by increasing the effective size of an antenna or by altering its radiation pattern. Impedance tuning aims to match the impedance

of the antenna to the impedance of the RF front-end to optimize the power transfer to the antenna. Successful matching improves TRP and TIS.

 $m V_{peak}$ specifies the maximum voltage the antenna tuner can withstand and still deliver acceptable harmonic performance. $m C_{off}$ is the capacitance presented by the antenna tuner while the tuner's switches are in the "off" state. Lower $m C_{off}$ increases the m Q of the tuner and affects antenna efficiency and effective tuning range. $m R_{on}$ is the resistance presented by the antenna tuner while the antenna tuner switches are "on." Lower $m R_{on}$ typically results in higher antenna efficiency, as well as improved TRP and TIS. High linearity switches are required to prevent degradation of TRP, TIS and carrier aggregation performance.

WHY IS V_{PEAK} IMPORTANT?

An antenna tuner may be thought of as a resonant circuit. The peak voltage inside a matching or resonant circuit can be much higher than at its input or output. This occurs because the internal impedance can be higher than 50 Ω , even if the input and output of the matching circuit are matched to 50 Ω . An aperture tuner is typically placed near the antenna, where the impedance

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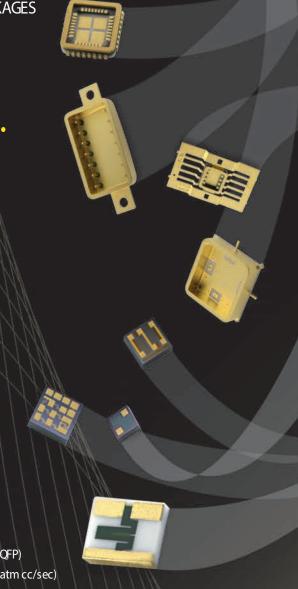
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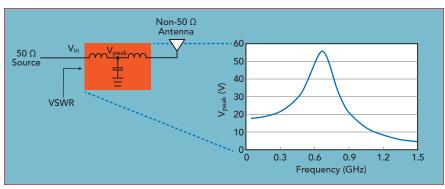


Fig. 1 Simplified aperture antenna (tuner installed directly on antenna radiating arm).

| TABLE 1 | | | | | |
|----------------|---------------------|-------------|-------------|--------------|--|
| Power (dBm) | V _{in} (V) | | | | |
| 35 | VSWR 1:1 | VSWR 2:1 | VSWR 5:1 | VSWR 10:1 | |
| | 18 | 24 | 25 | 32 | |

is generally higher than 50 Ω . The peak voltage on a tuning component depends on the input power level, the antenna or matching circuit topology and the loaded Q of the circuit. For example, at P_{in} = +35 dBm, the peak voltage across a shunt capacitor inside a matching circuit can be as high as 32 V (see Figure 1) and depends on the VSWR (see Table 1).

Aperture tuning consists of placing a tuning element in an appropriate location of the radiating structure, a location not directly connected to the matching circuit of the antenna feed. This guarantees the highest antenna radiated efficiency and prevents the feed

point impedance from changing during operation over the frequency spectrum. The V_{peak} required of an antenna tuner is determined by where the tuner is placed along the antenna and its proximity to the antenna's shorting pin (see Figure 2); V_{peak} is lower closer to the shorting pin and higher further from the shorting pin. Aperture tunability is most effective when the tuning element is placed in a location with the highest voltage distribution. Due to these factors, the maximum voltage present across an aperture tuner may be much higher than the voltage present at the antenna feed point.

The peak voltage of the antenna tuner is set by the division of RF voltage across the stack of FET switches in the antenna tuner design. Using an antenna tuner with insufficient V_{peak} for the application can result in permanent, catastrophic damage. Even if the tuner is not damaged, selecting a tuner with insufficient V_{peak} can significantly degrade TRP and TIS and lead to excessive harmonics, causing the phone to fail certification and delay product release. **DETERMINING THE**

APPROPRIATE TUNER

There are several considerations when selecting the appropriate aperture tuner. While R_{on}, C_{off} and V_{peak} are all critical parameters, the first step is determining the V_{peak} requirement. Tuning devices are used to set the resonant frequency and, as such, typically experience the highest voltage or highest current in the circuit. When V_{peak} is exceeded, the tuner begins a breakdown cycle, linearity deteriorates and the tuning switch emits potentially harmful harmonics. Selecting a tuner with insufficient V_{peak} will likely result in poor TRP and a failed radiated spurious emissions (RSE) certification.

V_{peak} cannot be measured on an antenna, because the act of measuring and touching the antenna changes its RF characteristics. The V_{peak} expected across the antenna tuner must, therefore, be simulated. Once defined, $\rm R_{on}$ and $\rm C_{off}$ are selected to achieve the TRP goal. This is also done through simulation. Depending on the specific antenna design and tuning bands, either R_{on} or Coff may have more influence on antenna efficiency.

DATA SHEET V_{PEAK}

The RF semiconductor industry has not converged on a common method for testing and specifying V_{peak}. Some suppliers simply specify a value in the absolute maximum ratings table of the data sheet. This is sufficient for describing the voltage beyond which the part may be damaged, but it does not guarantee that the part will perform adequately and not fail system-level RSE testing. Other suppliers may include a V_{peak} value in the electrical specifications table but do not indicate what level of performance is guaranteed. Designers must be certain sufficient performance is guaranteed when using a tuning device anywhere up to its V_{peak} level. The consequence of using a tuner above V_{peak} is that harmonics are injected into the system, which

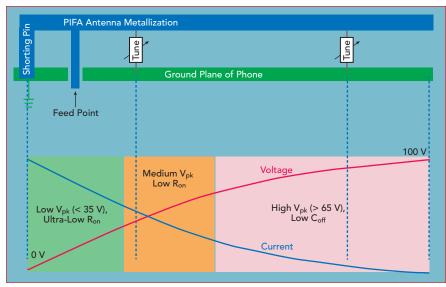


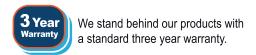
Fig. 2 Effect of the tuning element location on V_{peak}.

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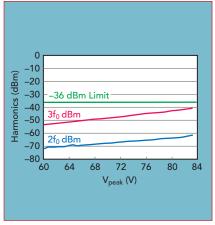
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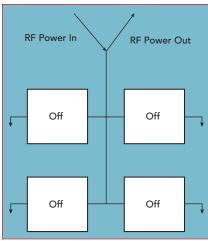
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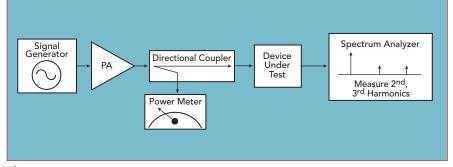
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🙏 Fig. 3 Skyworks' SPST antenna tuning V_{peak} .



 \bigwedge Fig. 5 $\rm\,V_{peak}$ is measured in the shunt configuration with all arms off.



ightharpoonup Fig. 4 V_{peak} measurement setup.

could result in excessive RSE and/or antenna efficiency to be lower than expected.

Skyworks uses harmonic performance to specify V_{peak} . Input power is swept and the second and third harmonics are measured. $V_{
m peak}$ on a Skyworks data sheet identifies the point where harmonics exceed -36 dBm, a level chosen to comply with the "3GPP Spurious Emissions Requirement" (Section 9.2). Spurious emissions are caused by unwanted transmitter effects such as harmonics, parasitics, intermodulation and frequency conversion, but they exclude out-of-band emissions. As one example, Skyworks' SKY19250 is a SPST antenna tuner with a rated V_{peak} of 80 V. Characterization test results are shown in Figure 3. Harmonic performance is better than -36 dBm beyond 80 V.

Skyworks uses a standardized V_{peak} measurement system (see Figure 4) for characterizing tuners. Peak voltage is verified by a highpower measurement in a 50 Ω en-

vironment and involves high-power levels that could destroy the device under test. To nondestructively measure V_{peak}, the antenna tuner is configured in a shunt configuration with all arms safely in the "off" state (see Figure 5).

SUMMARY

It is important to choose the correct aperture tuner component that meets R_{on} , C_{off} and V_{peak} criteria to match the antenna design. Antenna tuner V_{peak} is critical to the performance of the RF system. Using an antenna tuner with inadequate V_{peak} may result in poor TRP, TIS and certification failure. Simply relying on the V_{peak} in the absolute maximum ratings table of a data sheet is not sufficient. Harmonics are the best indicator of true V_{peak} performance and should be defined in the data sheet electrical specifications for V_{peak} . A well-calibrated V_{peak} measurement system must be used in order to safely and reliably test and select appropriate antenna tuner components.

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The innovative connector offers performance that, until recently, was not possible in such compact dimensions. A typical 2.2-5 flange saves up to 53 percent in space compared to the 4.3-10 and 70 percent versus the 7-16 connector (see Figure 1). From the tried and tested 4.3-10, the 2.2-5 uses the same designed plugs with three different locking types (see *Figure 2*), all of which can be used on the same jack:

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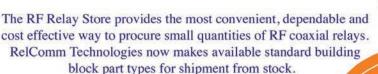
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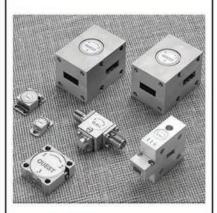


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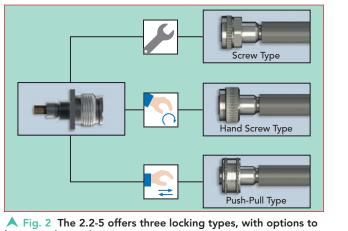
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GaN Front-End Module for X-Band Phased Arrays

Qorvo Greensboro, N.C.

mall size and component integration are key goals for high frequency phased array radars. As system frequencies increase, array element spacing reduces and the area for the RF front-end driving each element also shrinks. Addressing these needs, Qorvo's QPM1002 is a single-chip X-Band front-end module (FEM) for radar applications from 8.5 to 10.5 GHz. The MMIC integrates a T/R switch, low noise amplifier (LNA) and power amplifier (PA) on a single GaN MMIC (see **Figure 1**).

The QPM1002 is fabricated on Qorvo's 0.25 µm GaN on SiC process and encapsulated in a 5 mm × 5 mm plastic overmolded QFN, which minimizes cost, maximizes moisture robustness and simplifies next-level assembly. The compact size supports the tight lattice spacing of X-Band phased array radars and is also advantageous for electronic

warfare and communication systems.

In receive (Rx), the FEM provides 25 dB gain with a low noise figure of 2.2 dB (see *Figure 2*), with the typical input and output return loss around 13 and 12 dB, respectively. In transmit (Tx), the FEM has 33 dB small-signal gain and delivers 3 W saturated output power, 32 percent pow-

er-added efficiency and 25 dB large-signal gain (see *Figure 3*), with the typical input and output return loss 15 dB. The Rx and Tx performance include the losses and mismatch associated with the T/R switch. The MMIC includes an on-chip output power detector with a 0 to 0.3 V output proportional to transmit power. The FEM is robust and will handle up to 2 W power applied to the antenna port, eliminating the need for a limiter to protect the LNA in most systems. A photograph of the QPM1002 mounted on an evaluation board is shown in *Figure 4*.

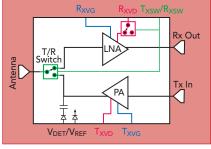
The QPM1002 is classified as EAR99 for export, meaning it can be exported to qualified international customers.

GaN ADVANTAGES

An all-GaN MMIC solution offers several advantages:

- GaN is robust, with an operating temperature range of -55°C to +100°C.
- GaN LNAs can survive high incident RF power, eliminating the need for an Rx limiter in front of the LNA.
- The all-GaN solution minimizes size and simplifies system integration.

Rx robustness was tested at 95°C by driving successively higher input power into the antenna port for three minutes at each power level. Based on test results, the QPM1002 has a maximum antenna port input power



▲ Fig. 1 The QPM1002 front-end integrates an LNA, PA and T/R switch and connects to the antenna.

Rogers' Laminates: Paving the way for tomorrow's Autonomous Vehicles

Autonomous "self-driving" vehicles are heading our way guided by a variety of sensors, such as short and long range radar, LIDAR, ultrasound and camera. Vehicles will be connected by vehicle-to-everything (V2X) technology. The electronic systems in autonomous vehicles will have high-performance RF antennas. Both radar and RF communication antennas will depend on performance possible with circuit materials from Rogers Corporation.

High-performance circuit laminates, such as RO3000® and RO4000® series materials, are already well established for radar antennas in automotive collision-avoidance radar systems at 24 and 77 GHz. To further enable autonomous driving, higher performance GPS/GNSS and V2X antennas will be needed, which can benefit from the cost-effective high performance of Kappa™ 438 and RO4000 series materials.

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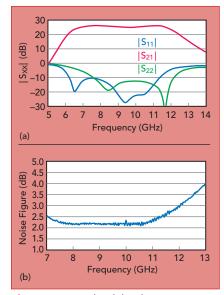
Short Range Radar

> Short/ Mid-Range

LIDAR

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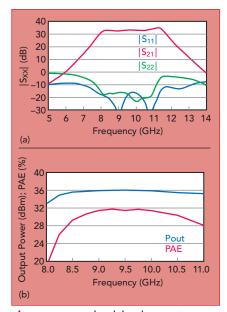
ProductFeature



ightharpoonup Fig. 2 Gain, $|S_{11}|$, $|S_{22}|$ (a) and noise figure (b) of the LNA path at 25°C.

rating of 2 W. PA robustness was similarly tested by driving it into saturation with highly reflective loads at the antenna port. The PA withstands a 10:1 load while driven into saturation without failure or degradation.

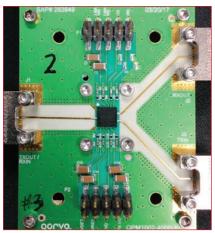
When the QPM1002 is in the Tx mode, on-chip circuitry turns off the current to the drain of the LNA using the Tx/Rx control lines (shown in Figure 1). This reduces the chance of LNA damage during Tx operation and increases the isolation of signals leaking through the LNA to the Rx output. The LNA turn-off circuitry conveniently eliminates the



ightharpoonup Fig. 3 Gain, $|S_{11}|$, $|S_{22}|$ (a) and output power and PAE (b) of the Tx path at 25°C.

need for gate/drain switching on the LNA when changing from Tx to Rx or vice-versa.

The typical output power of a GaN LNA is greater than 25 dBm, which could require attenuation or other power-limiting circuitry if downstream components are sensitive to power levels of this magnitude. To avoid this issue, the QPM1002 LNA implements a novel topology to limit the output power to 17 dBm, even when heavily saturated and at cold temperatures. This allows the LNA to directly drive sensitive SiGe beamformer ICs,



▲ Fig. 4 The QPM1002 surfacemounted to the evaluation board. A copper-filled via array underneath the module improves heat conduction from the device.

which typically have maximum input power ratings of 17 to 18 dBm.

OPTIMIZED ANTENNA PORT SWITCH

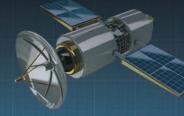
The T/R switch topology was optimized to minimize the Rx noise figure and maximize Tx power-added efficiency; both are heavily influenced by the respective networks interfacing with the SPDT switch. The best performance was achieved by absorbing the off-state switch capacitance into the PA output and LNA input matching networks.

Qorvo Greensboro, N.C. www.qorvo.com



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T&M Instrument Amplifiers Cover 700 MHz to 26.5 GHz

Maury Microwave Corp. Ontario, Calif.

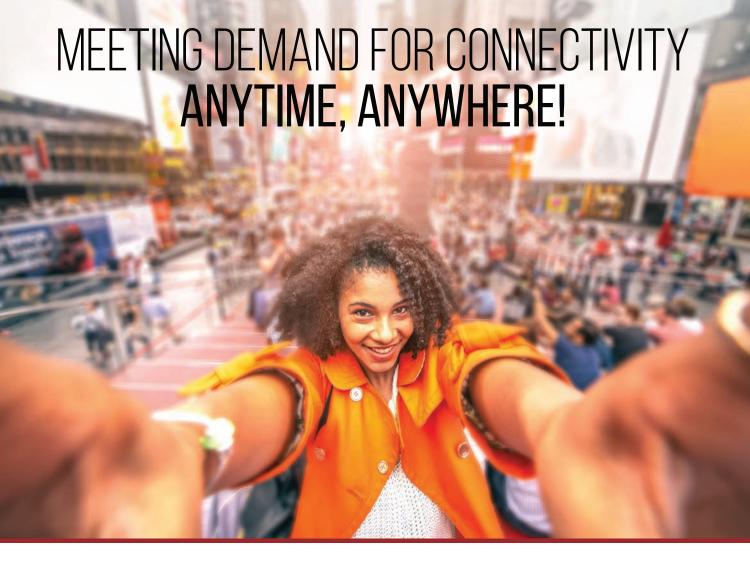
odern applications such as 5G, Wi-Fi and SATCOM require special attention when select-I ing suitable instrumentation and accessories to perform measurements for characterization, modeling, validation and design. One cannot simply use any available equipment but should select sources, analyzers and amplifiers with a high degree of linearity and sensitivity, to ensure signal fidelity and accurate, repeatable measurements. With these requirements in mind, Maury Microwave has released a line of test and measurement instrument amplifiers based on state-of-the-art, solid-state, GaN power amplifier (PA) modules to specifically address 50 and non-50 Ω measurements for modern applications, including 4G and 5G communications, advanced Wi-Fi standards, radar and SATCOM.

PERFORMANCE

Key features include high continuous saturated output power of 1 to 50 W across the

entire bands from 0.7 to 6, 2 to 6, 2 to 18, 6 to 18, 8 to 12 and 18 to 26.5 GHz. Maury Microwave MPA-series instrument amplifiers have high gain—between 30 and 50 dB, with a typical gain flatness of ±2 dB—to amplify the typical signal generator output power to the amplifier's rated saturated output. Users can manually adjust the gain over a range of 15 to 20 dB using the gain-adjustment knob on the front panel of the amplifier. All Maury amplifiers are unconditionally stable, and signal fidelity and accurate device-undertest measurements are ensured, due to low:

- Second harmonic output contribution of -35 to -15 dBc.
- Spurious signal contribution of -65 dBc at rated saturated output power.
- Third-order intermodulation products (IM3) of -48 to -33 dBc at 13 dB back-off with 10 MHz signal spacing.
- ACPR values of -50 to -40 dBc at 13 dB back-off typical, using an LTE signal with 20 MHz bandwidth and 9 dB peak-to-average ratio.



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▲ Fig. 1 The LCD display shows operating status, gain level and faults.

MPA-series amplifiers include an integrated LCD display indicating amplifier operating status, gain level and any faults recorded by the internal protection circuitry (see *Figure 1*). Fault protection includes automatic shut-off due to elevated temperature, fan failure and PA module over-current.

APPLICATIONS EXPERTISE AND RELIABILITY

MPA-series amplifiers have been created, in part, by leveraging Maury's 60+ year history in the RF/microwave industry and 30+ years of direct experience with transistor characterization, modeling, validation and PA



▲ Fig. 2 An MPA-series amplifier used in a vector-receiver load-pull system.

design. As application experts, Maury has manufactured, trained and supported turnkey measurement and modeling systems for 4G, 5G, Wi-Fi, radar and SATCOM applications, experiencing the pitfalls of using nonideal instruments and accessories and, conversely, the benefits of using ideal components. Using this experience, Maury specified and designed application-specific instrument amplifiers to act as the backbone of each measurement and modeling system (see Figure 2). Maury's unique insight from the application and user perspective enables its engineers to support the customer's entire test bench, not only the amplifier.



▲ Fig. 3 The MPA-series amplifiers are tested extensively, including harmonics, intermodulation and ACPR.

Maury MPA-series test and measurement instrument amplifiers are incredibly reliable, in part because of the advanced burn-in and aging procedures performed prior to final electrical test. The process includes exposing the amplifiers to extreme temperature conditions for prolonged duration, to identify premature component failure and mounting deficiencies. In addition, extended operation at the maximum saturated output power over the entire rated temperature range under CW and pulsed-CW operating conditions helps identify MMIC and PA module deficiencies or failures. After burn-in and aging, each instrument amplifier is tested using a state-of-the-art vector-receiver measurement system (see Figure 3). This system independently measures power at the fundamental, harmonic and intermodulation frequencies using single- and twotone input signals, as well as true ACPR using modulated wideband signals.

CUSTOM AND SEMI-CUSTOM

In addition to the standard offering, semi-custom models with variations on frequency range, power and gain are offered. Fully-custom amplifiers can also be developed, based on an extensive customer questionnaire covering frequency, output power, gain, harmonic power, spurious signals, intermodulation power, noise floor, mechanical dimensions, cooling requirements, etc.

Maury will release additional PAs during 2018 and 2019: 100 and 200 W between 0.7 and 2.7 GHz, higher power 18 to 26.5 and 26.5 to 40 GHz models.

Maury Microwave Corp. Ontario, Calif. www.maurymw.com



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High-Power Silicon Switches for Massive MIMO Front-Ends

Analog Devices Inc. Norwood, Mass.

IMO transceiver architectures are becoming widely used in the design of high-power RF wireless communication systems. As a step into the 5G era, massive MIMO (mMIMO) system covering the cellular bands are now being deployed in urban areas to meet the emerging demand for high data throughput and new services. The availability of highly integrated, single chip, baseband transceiver solutions, such as ADI's new ADRV9008/9 family of products, made this achievement possible. Similar integration is needed at the RF front-end of these systems to reduce power consumption for thermal management, shrink size, reduce cost and accommodate more MIMO channels.

MIMO architectures allow the RF output power and power handling requirements for amplifiers and switches to be relaxed. However, as the number of parallel transceiver channels increases, the complexity of peripheral circuits and total power consumption scales accordingly. ADI's new high-power switches, fabricated in silicon, are designed to simplify the RF front-end design, eliminating the need for peripheral circuits and reducing power consumption to a negligible level. ADI's high-power silicon switches offer RF designers and system architects the flexibility to increase system complexity without the RF front-end becoming a bottleneck in the design.

In time-division duplex (TDD) systems, a switch function is used at the antenna interface to isolate and protect the receiver input from the power of the transmitted signal. This switch can either be used directly at the antenna interface in relatively lower power systems (see *Figure 1*) or placed on the receive path for higher power applications, to ensure proper termination to the duplexer (see *Figure 2*). In both architectures, having a shunt arm on one of the switch outputs helps improve isolation.

PIN diode switches have been the preferred solution, offering low insertion loss and high-power handling. However, they need high bias voltages, to reverse bias for isolation, and high current, to forward bias for low insertion loss, which are shortcom-

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EuMW 2018 will see an estimated 1,500 conference delegates, over 4,000 attendees and in excess of 300 international exhibitors (inc. Asia & US).

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- MicroApps attend our annual European Microwave Week Microwave Application Seminars (MicroApps)

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| Exhibition Dates | Opening Time |
|--------------------------|---------------|
| Tuesday 25th September | 09:30 - 18:00 |
| Wednesday 26th September | 09:30 - 17:30 |
| Thursday 27th September | 09:30 - 16:30 |

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Don't miss Europe's premier microwave conference event. The 2018 week consists of three conferences and associated workshops:

- European Microwave Integrated Circuits Conference (EuMIC) 24th 25th September 2018
- European Microwave Conference (EuMC) 25th 27th September 2018
- European Radar Conference (EuRAD) 26th 28th September 2018
- Plus Workshops and Short Courses (From 23rd September 2018)
- In addition, EuMW 2018 will include, for the 9th year, the Defence, Security and Space Forum on 26th September 2018

The three conferences specifically target ground breaking innovation in microwave research. The presentations cover the latest trends in the field, driven by industry roadmaps. The result is three superb conferences created from the very best papers submitted. For the full conference programme including a detailed description of the conferences, workshops and short Courses, please visit www.eumweek.com. There you will also find details of our Partner Programme and other Social Events during the week...

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CONFERENCE PRICES

There are TWO different rates available for the EuMW conferences:

- ADVANCE DISCOUNTED RATE for all registrations up to and including 23rd August 2018
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Please see the Conference Registration Rates table on the back page for complete pricing information. All payments must be in Euro - cards will be debited in Euro.

Online registration is open now, up to and during the event until 28th September 2018

DELEGATES

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- · Register online at www.eumweek.com
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- · Alternatively, you can register onsite at the self service terminals during the registration opening times below:
 - Saturday 22nd September (16:00 19:00)
- Sunday 23rd September (08:00 17:00)
- Monday 24th September (08:00 17.00)
- Tuesday 25th September (08:00 17.00)
- Wednesday 26th September (08:00 17.00) Thursday 27th September (08:00 17.00)
- Friday 28th September (08:00 10.00)

Once you have collected your badge, you can collect the conference proceedings on USB stick and delegate bag for the conferences from the specified delegate bag area by scanning your badge.

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Register Online at www.eumweek.com

ONLINE registration is open from 28th May 2018 up to and during the event until 28th September 2018.

ONSITE registration is open from 16:00 on 22nd September 2018.

ADVANCE DISCOUNTED RATE (up to and including 23rd August) STANDARD RATE (from 24th August & Onsite).

Reduced rates are offered if you have society membership to any of the following*: EuMA, GAAS, IET or IEEE. EuMA membership fees: Professional €25/year, Student €15/year.

If you register for membership through the EuMW registration system, you will automatically be entitled to discounted member rates.

Reduced Rates for the conferences are also offered if you are a Student/Senior (Full-time students 30 years or younger and Seniors 65 or older as of 28th September 2018).

The fees shown below are invoiced in the name and on behalf of the European Microwave Association. EuMA's supplies of attendance fees in respect of the European Microwave Week 2018 are exempted from Spanish VAT.

ADVANCE REGISTRATION CONFERENCE FEES (UP TO AND INCLUDING 23RD AUG.)

| CONFERENCE FEES | AD | VANCE DISC | OUNTED | RATE |
|----------------------|-----------------------------------|-------------|------------|-------------|
| | Society Member (*any of above) | | Non Member | |
| 1 Conference | Standard | Student/Sr. | Standard | Student/Sr. |
| EuMC | €470 | €130 | €660 | €190 |
| EuMIC | €360 | €120 | €510 | €170 |
| EuRAD | €320 | €110 | €450 | €160 |
| 2 Conferences | | | | |
| EuMC + EuMIC | €670 | €250 | €940 | €360 |
| EuMC + EuRAD | €640 | €240 | €890 | €350 |
| EuMIC + EuRAD | €550 | €230 | €770 | €330 |
| 3 Conferences | | | | |
| EuMC + EuMIC + EuRAD | €810 | €360 | €1140 | €520 |

STANDARD REGISTRATION CONFERENCE FEES (FROM 24TH AUG. AND ONSITE)

| CONFERENCE FEES | ADVANCE DISCOUNTED RATE | | | | | |
|----------------------|-----------------------------------|-------------|------------|-------------|--|--|
| | Society Member (*any of above) | | Non Member | | | |
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| EuMC | €660 | €190 | €930 | €270 | | |
| EuMIC | €510 | €170 | €720 | €240 | | |
| EuRAD | €450 | €160 | €630 | €230 | | |
| 2 Conferences | | | | | | |
| EuMC + EuMIC | €940 | €360 | €1320 | €510 | | |
| EuMC + EuRAD | €890 | €350 | €1250 | €500 | | |
| EuMIC + EuRAD | €770 | €330 | €1080 | €470 | | |
| 3 Conferences | | | | | | |
| EuMC + EuMIC + EuRAD | €1140 | €520 | €1600 | €740 | | |

WORKSHOP AND SHORT COURSE FEES (ONE STANDARD RATE THROUGHOUT)

| FEES | | | | |
|---|-----------------------------------|------|------------|-------------|
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| Half day WITH Conference registration | €100 | €80 | €130 | €100 |
| Half day WITHOUT Conference registration | €130 | €100 | €170 | €130 |
| Full day WITH Conference registration | €140 | €110 | €180 | €130 |
| Full day WITHOUT Conference registration | €180 €140 | | €240 | €170 |

Other Items

PRIVATE VISIT TO THE THYSSEN-BORNESMIZA MUSEUM & COCKTAIL DINNER - 26TH SEPTEMBER 2018

Tickets for the private visit and cocktail dinner at the Thyssen-Bornesmiza Museum are offered at the price of € 45. Tickets are limited and available on a first-come, first-served basis.

DELEGATE LUNCHBOXES

Subsidised lunchboxes for delegates, WS/SC, doctoral and student school attendees are being offered by EuMW at the reduced cost of €5 per lunchbox (one per day).

Proceedings on USB Stick

All papers published for presentation at each conference will be on a USB stick, given out FREE with the delegate bags to those attending conferences. The cost for an additional USB stick is €50.

International Journal of Microwave and Wireless Technologies (8 issues per year)

International Journal combined with EuMA membership: €67 for Professionals or €57 for Students.

EUMW 2018 WORKSHOPS & SHORT COURSES

| SUNDAY 23rd September | | | | | | | |
|-----------------------|-------|------------|--|--|--|--|--|
| Full Day | WS-01 | EuMC/EuMIC | | | | | |
| Half Day AM | WS-02 | EuMC/EuMIC | | | | | |
| Half Day PM | WS-03 | EuMC/EuMIC | | | | | |
| Half Day AM | WS-04 | EuMC | | | | | |
| Half Day PM | WS-05 | EuMC | | | | | |
| Full Day | WS-06 | EuMC/EuMIC | | | | | |
| Half Day AM | WS-07 | EuMC | | | | | |
| Full Day | WS-08 | EuMC/EuMIC | | | | | |
| Full Day | WS-09 | EuMC/EuMIC | | | | | |
| Full Day | WS-10 | EuMC | | | | | |
| Full Day | WS-11 | EuMC/EuMIC | | | | | |
| Full Day | WS-12 | EuMC/EuMIC | | | | | |
| Half Day PM | SS-01 | EuMC/EuMIC | | | | | |
| Full Day | SS-02 | EuMC/EuMIC | | | | | |
| Full Day | SS-03 | EuMC/EuMIC | | | | | |

| THURSDAY 27th September | | | | | | | | |
|-------------------------|--|--|--|--|--|--|--|--|
| WTh-01 | EuMC | | | | | | | |
| WTh-02 | EuMC | | | | | | | |
| WTh-03 | EuRAD | | | | | | | |
| WTh-04 | EuMC/EuRAD | | | | | | | |
| WTh-05 | EuMC | | | | | | | |
| WTh-06 | EuMC | | | | | | | |
| WTh-07 | EuRAD | | | | | | | |
| | WTh-O1 WTh-O2 WTh-O3 WTh-O4 WTh-O5 | | | | | | | |

TUESDAY 25th September

WEDNESDAY 26th September
Half Day PM WW-01 EuMC/EuRAD
Full Day WW-02 FuRAD

Half Day PM WTu-01

| MONDAY 24th September | | | FRIDA | Y 28th Se | ptember |
|-----------------------|-------|------|-------------|-----------|------------|
| Full Day | WM-01 | EuMC | Half Day AM | WF-01 | EuRAD |
| Full Day | WM-02 | EuMC | Full Day | WF-02 | EuMC |
| Full Day | WM-03 | EuMC | Full Day | WF-03 | EuMC |
| Full Day | WM-04 | EuMC | Half Day AM | WF-04 | EuRAD |
| Full Day | SM-01 | EuMC | Full Day | WF-05 | EuMC |
| Full Day | SM-02 | EuMC | Full Day | WF-06 | EuMC |
| Full Day | SM-03 | EuMC | Full Day | WF-07 | EuMC |
| Full Day | SM-04 | EuMC | Half Day AM | SF-01 | EuMC/EuRAD |

| SPECIAL FORUMS & SESSIONS | | | | | | | | |
|--|---------------|---------------------------------------|----------------|--------------------------------------|---|--|--|--|
| Date | Time | Title | Location | No. of Days | f Days Fee | | | |
| Wednesday 26th September | 10:50 - 17:50 | Defence, Security & Space Forum | N101 + N102 | 1 | €20 for delegates (those registered for EuMC, EuMIC or EuRAD) | €60 for all others (those not registered for a conference) | | |
| Monday 24th - Wednesday 26th September | 08:30 - 17:50 | European Microwave Student School | N107 | One full day and two half-days | €40 | | | |
| Monday 24th - Wednesday 26th September | 08:30 - 17:50 | European Microwave Doctoral School | INIU8 | One full day and two half-days | ay 5 €80 | | | |

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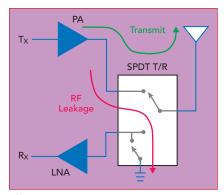


Fig. 1 Antenna switch.

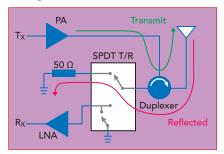


Fig. 2 LNA protection switch.

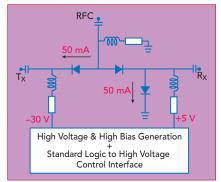


Fig. 3 PIN diode switch.

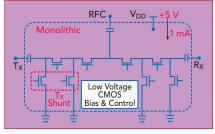


Fig. 4 Silicon switch.

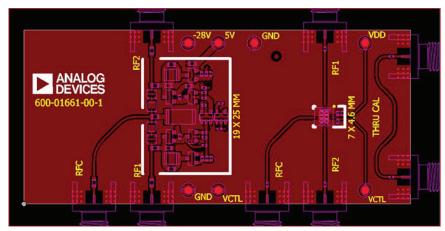


Fig. 5 PCB footprint comparison: PIN diode vs. silicon switch.

ings in mMIMO systems. Figure 3 shows a typical application circuit for a PIN diode switch, including the peripheral circuitry, where three discrete PIN diodes are biased through bias-tees and controlled with a high voltage interface circuit.

ADI's new high-power con switches are better suited to mMIMO designs. They are biased with a single 5 V supply, draw less than 1 mA current and do not need external components or interface circuits. The FET circuit architecture (see Figure 4) operates on low supply voltages and draws low bias currents, making the power consumption negligible and aiding system thermal management. Additionally, the FET architecture yields better isolation, as more shunt arms are incorporated on the RF signal path. ADI's silicon switches handle RF peak power up to 80 W, adequate margin to cover the peak-to-average power requirements for mMI-MO systems.

Figure 5 shows a side-by-side comparison of the PCB artwork on a single-layer design for a PIN diode switch and ADI's new silicon switch. The footprint of the silicon switch is

more than 10× smaller than the PIN diode switch footprint.

Table 1 shows ADI's family of high-power silicon switches, which are optimized for various power levels and package options. These devices reflect the intrinsic advantages of silicon technology: better ESD robustness and less part-to-part variation compared to alternative solutions.

As mMIMO systems evolve, they will need even higher levels of integration. ADI's new high-power silicon switch technology is well-suited for multi-chip module designs, enabling integration with LNAs to offer a complete single chip solution for TDD receiver front-ends. ADI plans to scale new designs to cover higher frequencies, leading to similar solutions for 5G mmWave systems. Other applications such as phased array radars will benefit from the advantages of the silicon switch architecture as ADI expands its product portfolio to X-Band and higher.

VENDORVIEW

Analog Devices Inc. Norwood, Mass. www.analog.com

| | TABLE 1 | | | | | | | | |
|-------------|--------------------|---|--------------------------------|----------------------|--------------------------------|----------------------|--|--|--|
| | | HIGH-POW | ER SILICON SWI | TCH FAMILY | | | | | |
| Part Number | Frequency (GHz) | Insertion Loss (dB) | Isolation (dB) | Average Power (W) | Peak Power (W) | Package Size (mm) | | | |
| ADRF5130 | 0.7 to 3.5 | 0.6 at 2.7 GHz 0.7 at 3.8 GHz | 45 at 3.8 GHz | 20 | 44 | 4 x 4 | | | |
| ADRF5132 | 0.7 to 5.0 | 0.60 at 2.7 GHz 0.65 at 3.8 GHz 0.90 at 5.0 GHz | 45 at 3.8 GHz 45 at 5.0 GHz | 3.2 | 20 at 3.8 GHz 10 at 5.0 GHz | 3 × 3 | | | |
| ADRF5160 | 0.7 to 4.0 | 0.8 at 2.7 GHz 0.9 at 3.8 GHz | 48 at 3.8 GHz | 40 | 88 | 5 × 5 | | | |



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zero span IF output, external triggering input, etc.



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TechBriefs



ini-Circuits and Vayyar Imaging, a 3D imaging sensor company, have partnered to transceiver project kits for students, university programs and hobbyists. The kits are developed to enable students to explore electromagnetic theory, RF/microwave engineering and applications such as radar. They address a significant gap in most university's RF/microwave programs, between textbook theory and the lab measurements to confirm the theory or evaluate the "real world" performance of RF/microwave components and systems.

The first kit, UVNA-63, enables students to build a fully functioning

DIY Vector Network Analyzer for Universities and Hobbyists

vector network analyzer (VNA), develop S-parameter algorithms and perform real-time measurements of two-port RF devices from 500 MHz to 6 GHz. The kit comprises Vayyar's high performance transceiver IC with RF components from Mini-Circuits and includes calibration standards, control software and a development environment for Python and MATLAB®.

The UVNA-63 VNA kit can be pre-ordered now from Mini-Circuits and will be delivered in September, coinciding with the fall semester at most schools.

Attendees at the upcoming EDI CON conference in Santa Clara will have the opportunity to play

with the DIY VNA at a workshop on Thursday morning, October 18. The hands-on "Build Your Own VNA" session, one of several EDI CON courses eligible for IEEE continuing education credits, will cover transmission line theory, the basics of S-parameter measurements and construction of a VNA. Participants will use the UVNA-63 kit to build a VNA, load the scripts, understand the math behind the measurements, make measurements and evaluate accuracy.



Mini-Circuits Brooklyn, N.Y. www.minicircuits.com



P Performance Antennas has developed a new series of dual sector antennas designed to reduce tower rental and installation costs by housing two or more antennas in a single radome. KP's new line comprises seven models, each consisting of two or more sector antennas inside a single, rugged radome. The antennas are offered with four or eight ports and support 2 x 2, 4 x 4 and 8 x 8 MIMO, depending on the model. The single mounting point reduces inches on the tower, lowers wind resistance and halves tower rental. The antennas also provide a rapid upgrade path to add frequency bands without installing more infrastructure.

Dual Sector Antennas Cover Bands from 2 through 6 GHz

The straight-on models in this line provide two forward-facing, high gain, 65 or 90 degree sector antennas in a single radome, one for each frequency band, and come in frequency combinations of 2 and 3 GHz, 2 and 5 GHz, 3 and 5 GHz and 5 and 5 GHz. They feature clean patterns and provide complete 360 degree coverage while minimizing interference. They also have mounting space for two ePMP radios, have four Type N female connectors and hot-dip galvanized steel sector brackets. These antennas are ideal for point-to-multipoint applications and support many of the popular radios in the WISP/WLAN market.

The side-angle models combine two 65 degree sector antennas in a single radome and mounted 60 degrees apart, with two ports angled at -60 degrees and the other two at +60 degrees, for a total of 120 degree coverage using two, 2 x 2 MIMO radios on a single antenna. These antennas achieve complete 360 degree coverage while minimizing interference, with only three side-angle sectors connected to six, 2 x 2 MIMO radios around a tower and ABCABC frequency reuse.

KP Performance Antennas Edmonton, Alberta, Canada www.kpperformance.com



he microwave industry lacks a suitable coaxial switch for frequencies above 30 GHz. Commercially available coaxial switches fall short in performance: they prove to be very lossy at high frequencies and cannot handle high power. Addressing this shortcoming, Sector Microwave Industries developed a new innovative technique that achieves the benefits of both coaxial and waveguide switches

Cowave: A Hybrid Coax-Waveguide Switch

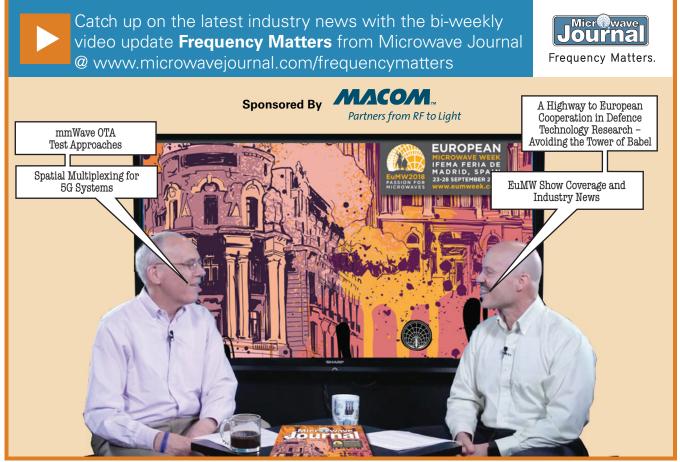
in a hybrid, "Cowave" switch. The Cowave switch is capable of handling high power and can be tuned by design to a wide band of waveguide frequencies up to 50 GHz.

The innovative aspect of this new switch is that it is contactless. The unit uses a miniature waveguide rotor and waveguide channels, enabling the transfer of energy inside the Cowave housing. The switch is compact and miniature compared to using coaxial-to-waveguide adapters with a typical waveguide

switch. The Cowave switch is also modular and can be configured to have different combinations of coaxial connectors and waveguide ports on both inputs and outputs to form DPDT, SPDT and more options.

Within the waveguide bandwidth, the switches typically measure 0.5 dB insertion loss, 1.25:1 VSWR and 45 dB isolation.

Sector Microwave Industries Deer Park, N.Y. www.sectormicrowave.com

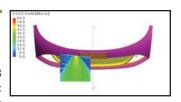


Software and Mobile Apps

2018 Versions of EM Simulation Software



Altair has released the 2018 versions of electromagnetic (EM) simulation software



FEKO®, WinProp®, Flux® and FluxMotor®. These EM solver tools, part of Altair's HyperWorks®, The Platform for Innovation™, are used to accelerate the global design process for the automotive, aerospace, defense, communications, consumer electronics, energy and healthcare industries. The 2018 release broadens functionality, simplifies workflows and enhances the user experience. For example, Flux 2018 brings new capabilities for CAD geometry simplification and meshing, improving workflow and increasing flexibility with the ability to solve faster in 3D using new HPC resources.

Altair Engineering Inc. https://altairhyperworks.com/

Filter Wizard®

K&L Microwave's Filter Wizard® filter synthesis and selection tool streamlines identification of filter products meeting customer specifications across a large portion of K&L's standard product offerings. Filter



Wizard® accelerates user progress from specification to RFQ for RF and microwave filters spanning an ever-increasing range of response types, bandwidths and unloaded Q values. Provide the application with your desired specifications, and the software will return a list of products that match, placing response graphs, outline drawings and downloadable S-parameters at your fingertips.

K&L Microwave www.klfilterwizard.com

The COMPLETE Library V18.1 VENDORVIEW Modelithics has released the

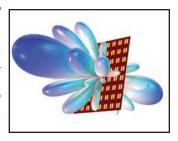
Modelithics has released the newest version, version 18.1, of the COMPLETE Library for use with NI AWR software. With this release, the Model-

ithics mmWave & 5G Library, a new product introduced in 2018, is now available for the NI AWR Design Environment® platform. With the addition of 47 new models, the library now represents over 16,000 components. Four significant new features have been incorporated into the v18.1 release as well. The release also includes the Modelithics mmWave & 5G library, with all models validated to at least 30 GHz, with some validated as high as 125 GHz.

Modelithics Inc. www.modelithics.com

Multiphysics® Software

COMSOL is a global provider of simulation software for product design and research. Its COMSOL Multiphysics® product is an integrated software environment for creating physics-based models and



simulation apps. A particular strength is its ability to model multiphysics systems. COMSOL users can convert their models into easy-to-use apps for their colleagues and customers worldwide. Apps are deployed and accessed online through the COMSOL ServerTM product. Interfacing tools enable the integration with all major technical computing and CAD tools.

COMSOL Inc. www.comsol.com

MegaPhase Connect App

Download MegaPhase's free iOS app, MegaPhase Connect, to help assist with daily calculations including wavelength, cable loss, insertion loss and



time delay. All test and measurement, RF cables and connector and adapters datasheets are accessible within the app, created specifically for engineers designing and building RF/microwave systems and components. Select the "MegaPhase Cable Builder" feature, which allows you to enter your specifications and render instant product offerings. The "My Products" feature allows you to save items of interest for future reference. Browse the updated brochure now available through the app.

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New Design Environment V14



NI AWR Design Environment V14 focuses on all stages of RF/microwave design with an emphasis on accelerating



design starts to address today's most challenging communications and aerospace/defense applications. Capabilities include powerful network synthesis for multi-band impedance matching circuits, advanced layout editing capabilities for PCB/module EM verification, design support for phased-array antenna configuration/optimization and enhanced analysis, automation and report/measurement management.

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Presented by: John Coonrod, Technical Marketing Manager, Rogers Corporation, Advanced Connectivity Solutions

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NEW PRODUCTS

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Centric RF

1.85 mm F/F 67 GHz Flanged Adapter



Centric RF announced a 4-hole flanged adapter covering the full IEEE P287 bandwidth of 0 to 67 GHz. The C8064 is a 1.85 mm female to female adapter with a

4-hole flange featuring a stainless steel body and BeCu female contacts. Maximum VSWR is 1.25 from 0 to 67 GHz. The 67 GHz performance allows usage in some of the new Wi-Fi bands which can extend to 66 GHz. Availability is from stock, pricing is \$355 for 1-9.

www.centricrf.com

Ceyear

VENDOR**VIEW**Solid-State Amplifiers



Ceyear announced their new line of solid-state amplifiers. These are offered in banded solutions from 9 kHz to 110

GHz and power levels reaching as high as 200 W. These amplifiers are highly accurate using internal RF power monitoring and superior cooling. This new amplifier line offers top level quality at an affordable price to all RF designers. Prices start at \$22,500. www.topdogtest.com/ceyear

Custom MMIC

VENDORVIEW GaAs Low Noise Amplifier



Custom MMIC now offers a new GaAs Low Noise Amplifier (LNA) MMIC with broadband noise figure performance previously only achievable with

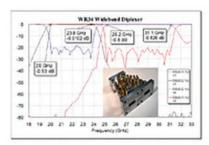
discrete FET designs. The CMD283C3, with 0.6 dB noise figure, is the first in a family of new ultra-low noise amplifiers. The CMD283C3 LNA covers 2 to 6 GHz with high midband gain of 27 dB and output P1dB of 16 dBm.

www.custommmic.com/cmd283c3-low-noise-amplifier/

Exceed Microwave

VENDOR**VIEW**Wideband Waveguide Diplexer

Exceed Microwave's WC-Series waveguide diplexers can provide very wide passbands and also comes in small sizes. DPX-WC-22-28-34 is a WR34 diplexer cover-



ing nearly the entire waveguide operating frequency band. Each channel bandwidth of DPX-WC-22-28-34 is roughly 20 percent while maintaining very good return loss at all ports. The size is only 1.5 in. × 1.8 in. × 0.9 in., which allows waveguide assemblies to be compact. WC-Series diplexers are available in different waveguide sizes. Exceed Microwave designs and manufactures high performance waveguide and coaxial filters.

www.exceedmicrowave.com

Fairview Microwave Inc. Gold-Plated 4-in-1 SOLT Calibration Kits



Fairview Microwave Inc. has launched a new line of 4-in-1 3.5 mm calibration kits for cable verification, antenna measurement and other field test and measure-

ment applications. Fairview Microwave's new line of integrated, short-open-load-through (SOLT) calibration kits is made up of two models that have a 26.5 GHz calibration capability. They feature a compact, lightweight, 4-in-1 design package with gold-plated, 3.5 mm connectors and a convenient lanyard. Plus, they are available off-the-shelf with same-day shipping.

www.fairviewmicrowave.com

Kaelus Battery Operated PIM Analyzer



The iPA Series passive intermodulation (PIM) analyzer from Kaelus is the first battery powered PIM test analyzer versatile enough to support multiple test

scenarios such as testing at the top of the tower, base of tower, rooftop and in-building for DAS systems. This IEC compliant 20 W, rugged, battery operated analyzer includes a tablet computer in a ruggedized case for remote control. This allows hands-free dynamic testing that is safe and convenient. www.kaelus.com

MCV Microwave VENDORVIEW Ultra-Low PIM Cavity Filters and Multiplexers



MCV Microwave has developed a new line of ultra-low passive intermodulation (PIM) cavity filters and

multiplexers covering the TETRA and all LTE frequency bands from 300 to 3600 MHz. The typical production PIM performance is -163 dBc, measured with two CW tones, each at 43 dBm. An even lower PIM filter line with a guaranteed -173 dBc is available for PIM test bench and more demanding testing applications.

www.mcv-microwave.com

Mini-Circuits

WENDORVIEW MMIC Amplifier



Mini-Circuits' PHA-23HLN+ ultra-high dynamic range MMIC amplifier sets the new industry standard for noise figure and IP3 in VHF/ UHF communications.

This model is well matched to 50 Ω from 30 MHz to 2 GHz and provides 1.4 dB noise figure, +44.4 dBm IP3, making it ideal for maximizing sensitivity and dynamic range in high performance receiver applications. It delivers 21 dB typical gain with ±1.8 dB flatness, +28.4 dBm output power at 1 dB compression. The amplifier is fabricated using E-PHEMT technology with excellent repeatability.

www.minicircuits.com

MiniRF VENDORVIEW Transformers



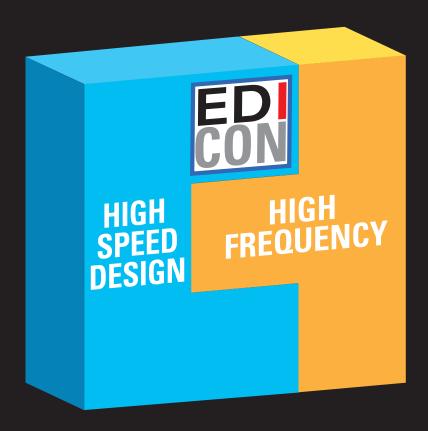
The MRFXF0024 transformer is designed for applications that require very small, low cost and highly reliable surface mount components.

Applications may be found in broadband, wireless and other communications systems. These units are built lead-free and RoHS compliant and feature welded wire construction for increased reliability. S-parameters are available on request.

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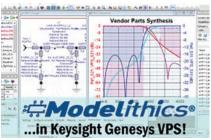


NewProducts

Modelithics



The Modelithics® COMPLETE Library v18.2



The 2018 version of the Modelithics COMPLETE Library for Keysight Genesys is now available. Modelithics models play a key part in the new Vendor Parts Synthesis (VPS) tool in Genesys software. VPS utilizes the scalability features of

Modelithics models to allow complete design synthesis in a simple, streamlined process. Once goals are set for a specific design, VPS incorporates Modelithics models to accurately account for parasitics and optimize the design using the over 16,000 commercially available vendor components represented in the Modelithics library. www.modelithics.com

Pasternack



40 GHz Skew Matched Cable Pairs



Pasternack has launched a new line of skew matched cables for use in high speed digital tests of 10 to 28 Gbps, including differential signals, bit-error-rate testing and eye diagrams. Pasternack's new line of skew matched cables is made up of three new models that are extremely flexible and have 1

ps delay match. These cables deliver excellent VSWR of 1.4:1 and are 100 percent tested for skew match.

www.pasternack.com

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Reactel manufactures a line of filters, multiplexers and multifunction assemblies covering up to 50 GHz. From small, lightweight units suitable for flight or portable systems to high-power units capable of handling up to 25 kW, connectorized or

surface mount—the company's talented engineers can design a unit specifically for your application.

www.reactel.com

Richardson RFPD

Wideband RF Transceiver



Analog Devices' ADRV9009 is the only transceiver with the bandwidth and RF performance to create a clear path to 5G, and the versatility to support all 2G, 3G and 4G cellular standards. Features include 75 MHz to 6 GHz, 200 MHz bandwidth dual transceiver, common platform design for

2G/3G/4G/5G, system integration replaces up to 20 components, significantly reducing SWaP, simplified digital beamforming through internal LO phase synchronization and fast frequency-hopping.

www.richardsonrfpd.com

RLC Electronics Inc.

Surface Mount Product Enhancements



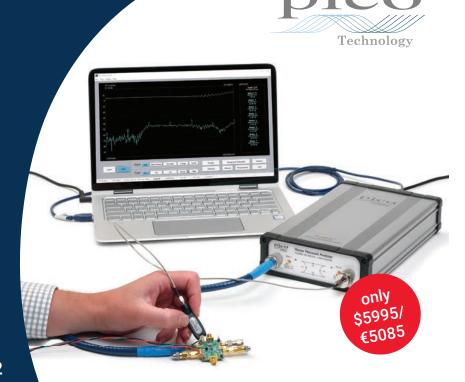
RLC Electronics continues to invest in its surface mount technology to add to its extensive capabilities across multiple product lines. These parts are ideal for the latest aerospace and

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NewProducts

defense platforms, which utilize surface mount components to reduce size, overall footprint and integration time and, most importantly, cost. The company's surface mount electromechanical switch product enhancements include both SPDT and DPDT offerings, operating up to as high as 26.5 GHz.

www.rlcelectronics.com

SAGE Millimeter VENDORVIEW Rotary Vane Attenuator



Model STA-60-12-D8 is an instrumentation grade, high precision and high attenuation range direct reading, rotary vane attenuator

for use in mmWave test sets across the standard E-Band frequency range of 60 to 90 GHz. The attenuator has a large scale calibrated dial which indicates the attenuation value directly. The attenuator is an ideal piece of equipment in waveguide systems where a broad direct reading of attenuation is required. The attenuator exhibits exceptional repeatability during frequent attenuation setting operations.

www.sagemillimeter.com

W. L. Gore & Associates PHASEFLEX® Microwave / RF Test **Assemblies**



W. L. Gore & Associates has introduced the new GORE®PHASEFLEX® Microwave/RF Test Assemblies, Type ON for high density test/

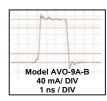
interconnection—a lightweight assembly that ensures consistent, repeatable measurements with stable electrical performance up to 50 GHz. High-density and modular test instruments for wireless devices and aerospace systems have become increasingly complex, with a larger number of ports that can accept up to 32 test assemblies or more.

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> Avtech Electrosystems Ltd. http://www.avtechpulse.com/



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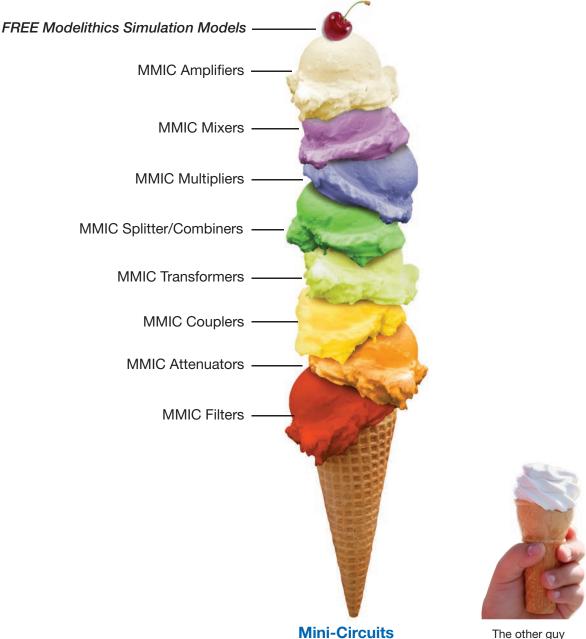
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AT&T's 5G Lab Lays the Foundation for 5G







ollowing the approval of the 5G New Radio (NR) non-standalone specification in December and the standalone specification in June, 5G is quickly, although quietly, being deployed, moving from modest lab and field trials to what will become highly visible commercial offerings to paying customers in often non-ideal environments: cities, towns and rural stretches with leaves, rain and snow, energy-efficient glass, moving vehicles and non-line-of-sight links. Turning the academic theory of 5G into the promises we read about—multi-Gbps broadband, connected and autonomous vehicles, nearly every object sending data to the cloud—offers both potential and challenge, causing mobile operators to invest billions in this next-generation network.

AT&T, serving some 90 million U.S. subscribers, has declared it will be the first to deploy mobile 5G by the end of 2018, fully conforming to the 3GPP standard, operating at mmWave frequencies and initially in 12 U.S. cities. As 5G smartphones will not yet be available, early adopters will use 5G "pucks" tethered via Wi-Fi to their existing phones or computers. The infrastructure hardware is frozen and now being deployed, although the software will be updated as the 5G standard evolves.

This commercial 5G launch will take the efforts of thousands of AT&T employees, following hundreds doing the R&D to establish feasibility and define the network architecture. One core team behind this effort has been a dozen or so engineers in Austin, led by David Wolter. Known as the 5G Lab, the team's mission was to evaluate the architectural trade-offs to optimize the system-level performance of AT&T's 5G network. The first step: understanding the propagation characteristics of the new frequency bands. The team combined simulation using internally-developed tools with measured data to model link performance. The

next step: extending the analysis to assess and optimize network performance.

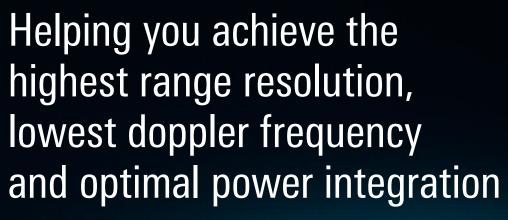
Key to making 5G robust—and much of the fun and gratification from the role—comes from conducting measurements in the field. To help characterize propagation, the 5G Lab developed the "Porcupine," a channel sounder that acquires and processes data in real-time, which the lab uses to develop channel models for office, outdoor and arena environments. From their nine-story office building, the team tests links to beta 5G users at nearby businesses, apartments and a church, as well as performing drive testing along a mile-long route around the building. Data collected from these nearby tests has been supplemented with field trials in Kalamazoo, South Bend and Waco. To acquire more real world data, AT&T is building a larger test site at another location, with more telephone poles for mounting small cells and a longer road for testing V2X and autonomous vehicles.

Among its duties, the 5G Lab provides data and recommendations to support AT&T's standardization efforts with the 3GPP, other bodies and industry groups such as the NYU Wireless 5G Summit. The team has contributed more than 330 technical papers and been granted 15 essential patents.

The Lab maintains close relationships with network equipment manufacturers such as Ericsson and Nokia, to keep abreast of and steer their developments. The team also devotes time to the component companies developing the building blocks for 5G, as it's vital to understand the capabilities of the underlying technologies—particularly considering the nascent maturity of mmWave.

While the world awaits 5G, much of the 5G Lab's work is complete. Confident that the technology will work, the team is looking to the next challenge. Is it too soon to say 6G?

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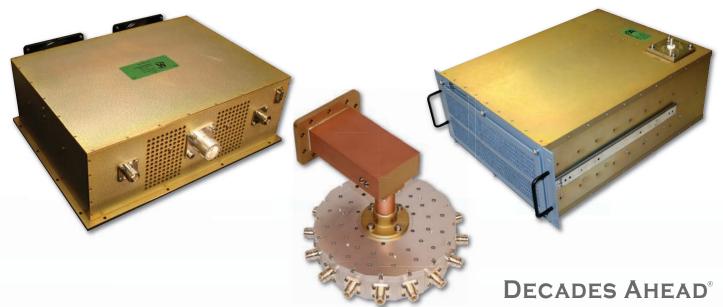




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